### NASA's Electical Power-Only Steam Analysis

New Energy Times received this document in a PowerPoint file format on July 22, 2011 from Michael A. Nelson of NASA's Marshall Space Flight Center.

One of Nelson's staff members prepared this document, however, the staff member asked to remain anonymous. We agreed because we have confirmed Nelson's identity, we consider his staff member's information useful, and Rossi has recently publicly threatened and attempted to intimidate several qualified critics.

The dialouge in the yellow boxes was written by Nelson.

## Rossi Device Analysis Assuming No Ni-H Participation

# July 20, 2011

WATER FLOW = 
$$3 kg/h = 3 kg/h$$
  
VADRIZATION HEAT = 615.6 wh/kg  
EMERGY PROCEP:  
 $615.6 \times 7 = 4,309.2$  wh  
 $AT 100.1 C = 25.3 = 74.3 km/h$   
(BECAUSE THE SIECHIC HEAT OF  $H_{0} = 1$ )  
 $Kod = 1.44$  wh  $\rightarrow 34.8$  kods  $35.2$  wh  
 $85.2 \times 7 = 5.96.3$   
THEREFORE THE FOTAL ENGRAY PROJECT IS  
 $4,309.2 + 6,536.9 = 4,306.4$  wh/h  
ENERCY CONSUMED:  
 $3.5 A \times 210 V = 770$  wh/h  
 $4,906.1 = 6.37$   
 $720$   
New Energy Times

From Rossi's notes:

Start with information from Rossi's notes and assuming no heat from a LENR process. Determine what quality of steam can be produced if the only input power in is the 770 W heating element built into Rossi's device.

Assume that the heat exchanger for the resistance heater is 100% efficient.

Input Power = 770 W = 0.77 kJ/sec

What happens if I add 770 W to water in a pipe flowing at 7 kg/hr (1.944e-3 kg/sec)?



Assume:

-1 atm (constant pressure process)

- steady-state (mass in = mass out)

Treat Rossi's device like a pipe, as shown above, with water flowing in one end of the pipe. Steam of some unknown quality is flowing out the other end.

Starting temperature of the water flowing in is given by Rossi. The rate of heat into the volume of water internal to the device is Qdot. The mass flow through the device is Mdot. Constant pressure of 1 atmosphere on water flow in and out of the device.



 $h_{out} = 502.26 \frac{kJ}{ka}$ 

Steady-state, no work.

Use the first law of thermodynamics. Solve for the enthalpy of the water mass exiting the device. This is an abbreviated expression of the 1st law with the kinetic and potential energy of the system already zeroed out. Also terms related to work done by the system are zeroed out since no work is being done.

From REFPROP v8, water at P=1 atm, T= 25.3 °C,  $h_{in}$  = 106.17 kJ/kg

$$h_{out} = \frac{\dot{Q} + \dot{m}h_{in}}{\dot{m}}$$

$$h_{out} = \frac{0.77 \frac{kJ}{\sec} + \left(1.944e - 3\frac{kg}{\sec}\right) \left(106.17 \frac{kJ}{kg}\right)}{\left(1.944e - 3\frac{kg}{\sec}\right)}$$

K	4: water: Specified state points													
		Temperature (°C)	Pressure (atm)	Density (kg/cm³)	Volume (cm³/kg)	Enthalpy (kJ/kg)	Quality (kg/kg)	Therm. Cond. (mW/m-K)	Viscosity (µPa-s)	Prandtl				
	1	25.300	1.0000	0.00099697	1003.0	106.17	Subcooled	607.71	884.04	6.0824				
	2	99.974	1.0000	0.000015949	62700.	502.26	0.036873	Undefined	Undefined	Undefined				
	3													

Adding 770 W to 25.3 C water flowing at 7 kg/hr at 1 atm will yield saturated water at a quality of 0.037 or 3.7 % vapor <u>by mass</u>.

#### Saturation properties at 1 atm (for later use)

K	🖆 5: water: Saturation points (at equilibrium)												
		Temperature (°C)	Pressure (atm)	Liquid Density (kg/cm³)	Vapor Density (kg/cm®)	Liquid Volume (cm <sup>s</sup> /kg)	Vapor Volume (cm³/kg)	Liquid Enthalpy (kJ/kg)	Vapor Enthalpy (kJ/kg)				
	1	99.974	1.0000	0.00095837	0.00000059766	1043.4	1673200.	419.06	2675.5				
	2												

(See next page for dialogue)

Use the specified state points feature of the Reference Properties (REFPROP) database that is available from the National Institute for Standards and Technology (NIST). Plug in any two pieces of information about water and it will give you all other properties for those two pieces of information.

Plug in the pressure and enthalpy of water. It will give you the quality of the water by mass as well as other properties that you choose under your REFPROP options. The quality given is defined as the mass of the vapor divided by the mass of the vapor plus the mass of the liquid of the water exiting the device.

Switch to the saturated points properties table in REFPROP (since we know the water has reached its saturation temperature because it is boiling inside the device). You can use a single property to obtain all other properties of water in a saturated state. In this case we want to know the density of water vapor and water liquid at saturation for 1 atmosphere so we can show how the mass quality of the output steam compares to the volume quality of output steam.

#### Quality (x) is defined as:





Start with the definition of steam quality by mass. State all mass in terms of volume and density. Now define what is meant by quality of steam in terms of volume with a variable y.

Substitute the term for quality of steam by volume into the expression for quality of steam by mass.

NOTE: I cannot tell you that there is such a term called "quality of steam by volume" in any text book anywhere on this subject. I'm just telling you what we've defined it as. You can substitute the phrase "fraction of vapor by volume" if its inappropriate to say quality by volume.

$$Define \_vapor \_volume \_ fraction \_as: y = \frac{V_{vapor}}{V_{total}}$$

$$x = \frac{\rho_{vapor} y}{\rho_{liquid} (1 - y) + \rho_{vapor} y}$$



### Solve this equation for y

Express the term for quality of steam by volume in terms of the quality of steam by mass and the density of both the liquid and vapor at the saturation point for one atmosphere.

Volume fraction of vapor can then be determined from mass quality (x) and the saturated liquid and vapor densities.

#### 🐴 4: water: Specified state points

	Temperature (°C)	Pressure (atm)	Density (kg/cm³)	Volume (cm³/kg)	Enthalpy (kJ/kg)	Quality (kg/kg)	Therm. Cond. (mW/m-K)	Viscosity (µPa-s)	Prandtl
1	25.300	1.0000	0.00099697	1003.0	106.17	Subcooled	607.71	884.04	6.0824
2	99.974	1.0000	0.000015949	62700.	502.26	0.036873	Undefined	Undefined	Undefined
3					L				

🖀 5: water: Saturation points (at equilibrium)

<b>v</b> —	$x ho_{liquid}$					
<i>y</i> –	$(1-x)\rho_{vapor} + x\rho_{liquid}$					

	Temperature (°C)	Pressure (atm)	Liquid Density (kg/cm³)	Vapor Density (kg/cm³)	Liquid Volume (cm³/kg)	Vapor Volume (cm³/kg)	Liquid Enthalpy (kJ/kg)	Vapor Enthalpy (kJ/kg)
1	99.974	1.0000	0.00095837	0.00000059766	1043.4	1673200.	419.06	2675.5
2								

$$\rho_{liquid} = 0.00095837 \frac{kg}{cm^3}$$
$$\rho_{vapor} = 0.00000059766 \frac{kg}{cm^3}$$

y = 0.984

x = 0.036873

Adding 770 W to 7 kg/hr water flow will produce 3.7 % vapor <u>by mass</u>, but 98.4% vapor <u>by volume</u>.

Plug in the values for quality by mass and liquid density of water at saturation and the vapor density of water at saturation from REFPROP. You get the quality of the steam by volume.

As stated above, an input energy of 770 W can yield steam with a vapor fraction of 98.4 % by volume.

This is because the expansion fraction of water under one atmosphere of pressure at saturation temperature from liquid to vapor is 1603.6036.















#### Summary:

Heat input from heater alone will create 98% vapor by volume.

Accurately measuring steam quality at the exit of the device is vital to understanding the performance of the device. Temperature alone will not suffice.