

# PRECISION AND ACCURACY OF COLD FUSION CALORIMETRY

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# OBJECTIVES

## Establish Thermal Balance For A Blank System (Pt/D<sub>2</sub>O)

(0.01% Error)

- Precision of  $\pm 0.1$  mW for 800 mW Input
- Measure Excess Power From Oxygen Reduction  
(Recombination)

(1.1 mW)

## Compare With Pd-B/D<sub>2</sub>O System

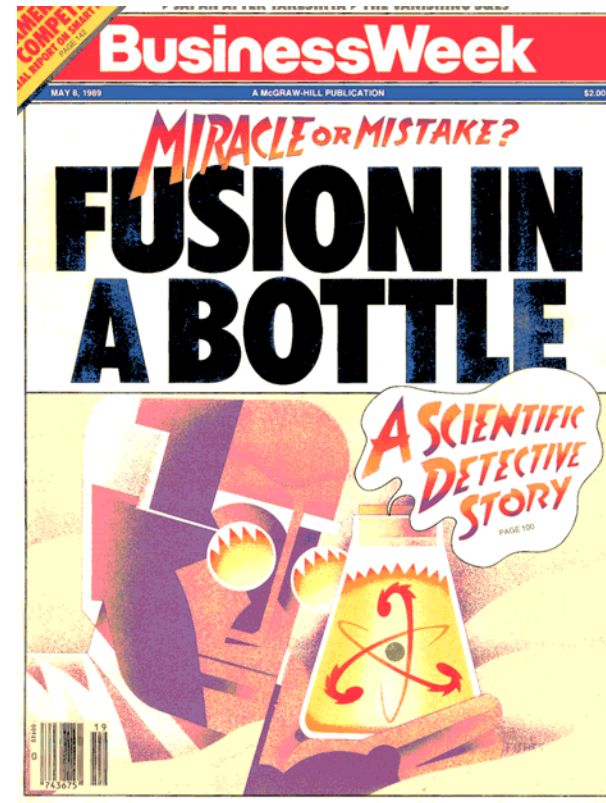
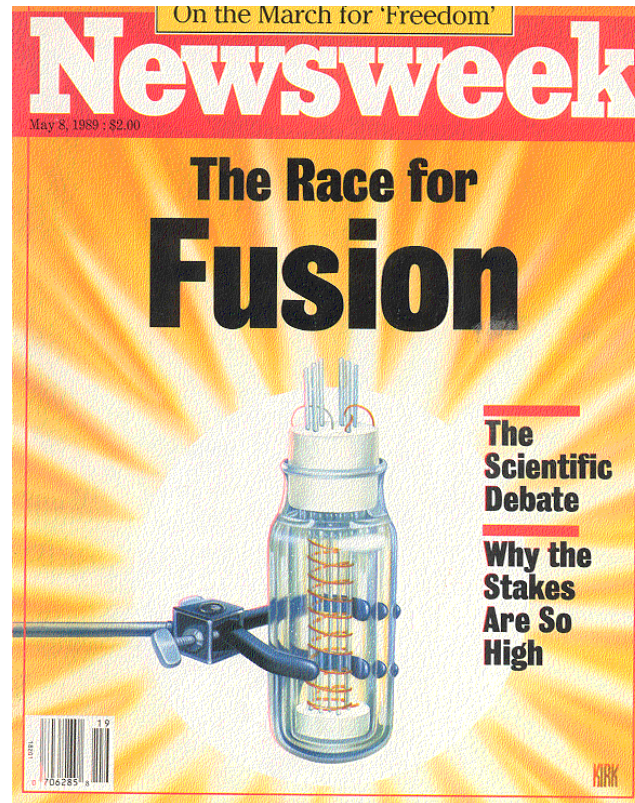
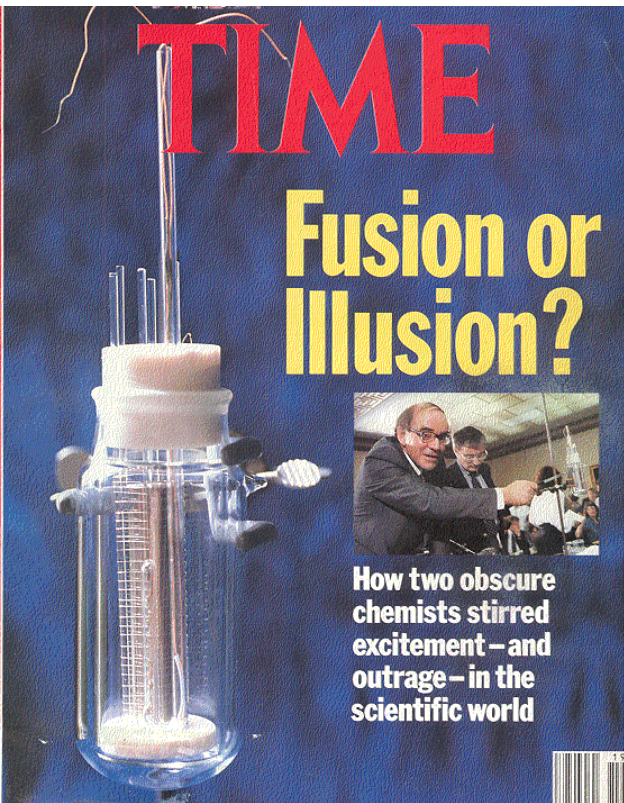
- Excess Power of 50 to 500 mW
- Increase of Excess Power to 10 W During Boil-Off

## Explain The Different Behavior of Pt/D<sub>2</sub>O and Pd-B/D<sub>2</sub>O



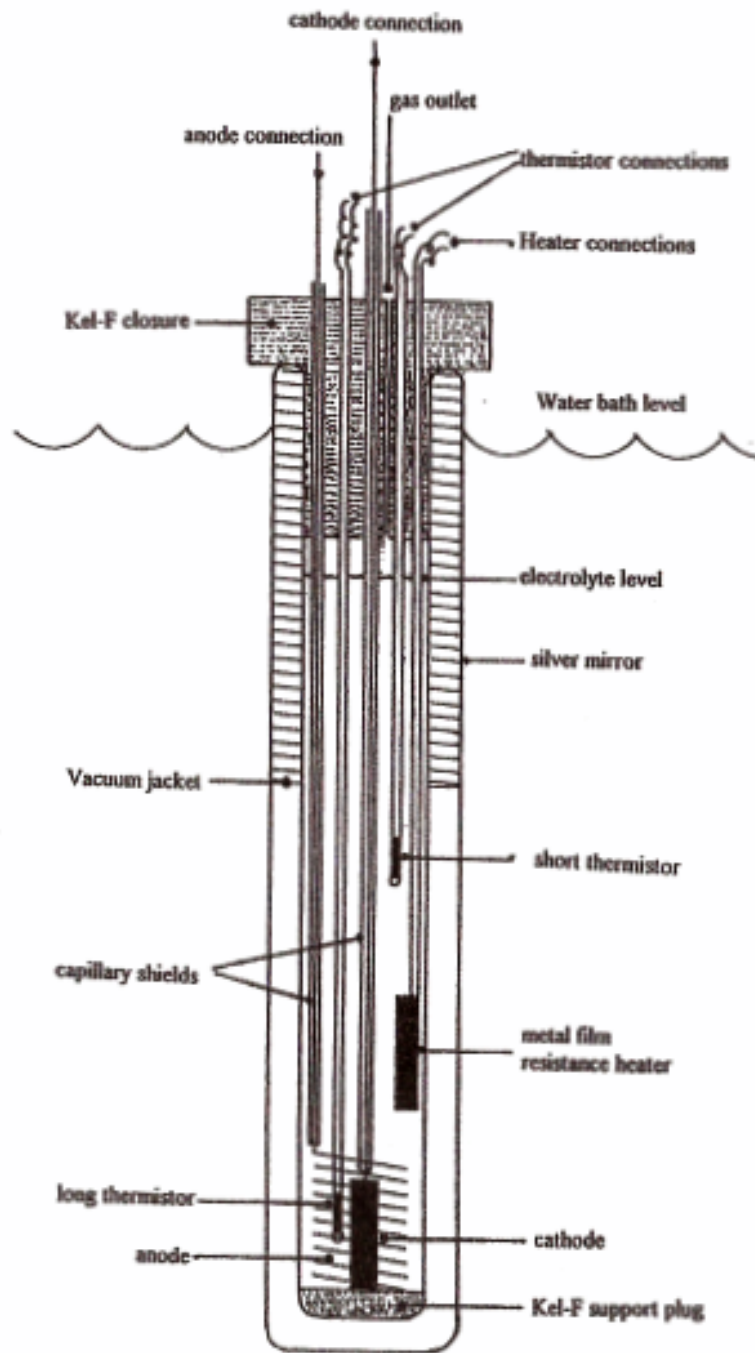
# Magazine Cover Stories

## 8 May 1989



*TRULY EXTRAORDINARY INTEREST*

# Isoperibolic Dewar Calorimetry Cell



# FUSION ENERGY CALCULATION



$$(1.5 \times 10^{43} \text{ D atoms}) \left( \frac{1_{\text{fusion}}}{2_{\text{Datom}}} \right) (23.8 \times 10^6 \frac{\text{eV}}{\text{fusion}}) (1.602 \times 10^{-19} \frac{\text{J}}{\text{eV}}) = 2.9 \times 10^{31} \text{ J}$$

## Energy per person per year (USA)

$$(10.0 \frac{\text{kW}}{\text{person}}) (1000 \frac{\text{W}}{\text{kW}}) (365 \frac{\text{days}}{\text{year}}) (24 \text{ hr/day}) (60 \text{ min/hr}) (60 \text{ s/min}) = 3.15 \times 10^{11} \text{ J}$$

## World (7 billion) Energy per year

$$(7 \times 10^9) (3.15 \times 10^{11} \text{ J}) = 2.2 \times 10^{21} \text{ J/year}$$

## Years Fueled by D + D Fusion

$$(2.9 \times 10^{31} \text{ J}) / (2.2 \times 10^{21} \text{ J/year}) = 1.3 \times 10^{10} \text{ years}$$

(13 billion years!)

# HEAT TRANSFER PATHWAYS

## POWER (J/S OR W)

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**Calorimetric System,  $P_{\text{calor}}$**

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**Electrochemical Power,  $P_{\text{EI}}$**

**In-Cell Heater Power,  $P_{\text{H}}$**

**Anomalous Excess Power,  $P_{\text{X}}$**

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**Gas Evolution Power,  $P_{\text{gas}}$**

**Heat Radiation Power,  $P_{\text{R}}$**

**Heat Conduction Power,  $P_{\text{C}}$**

**Rate of Work Done By Gases,  $P_{\text{W}}$**

# CALORIMETRIC EQUATIONS

## (First Law of Thermodynamics)



$$P_{\text{calor}} = P_{\text{EI}} + P_{\text{H}} + P_{\text{X}} + P_{\text{gas}} + P_{\text{R}} + P_{\text{C}} + P_{\text{W}}$$

where

$$P_{\text{calor}} = C_p M (d T_{\text{cell}}/dt)$$

$$P_{\text{EI}} = (E(t) - E_{\text{H}}) I$$

$$P_{\text{gas}} = -(I/F) \{ [0.5 C_{p,D_2} + 0.25 C_{p,O_2} + 0.75 (P/(P^* - P)) C_{p,D_2O(v)}] \Delta T + 0.75 (P/(P^* - P)) L \}$$

$$P_{\text{R}} = -k_{\text{R}} f(T) \text{ where } f(T) = T_{\text{cell}}^4 - T_{\text{b}}^4$$

$$P_{\text{C}} = -k_{\text{C}} (T_{\text{cell}} - T_{\text{b}})$$

$$P_{\text{W}} = -RT (dn_{\text{g}}/dt) = -RT (0.75 I/F)$$



# FLEISCHMANN'S DEWAR CALORIMETRY

$$P_R \gg (P_C + P_W)$$
$$P'_R = P_R + P_C + P_W = -k'_R f(T)$$

Thus

$$P_{calor} = P_{EI} + P_H + P_X + P_{gas} + P'_R = P_{EI} + P_H + P_X + P_{gas} - k'_R f(T)$$

Lower Bound Heat Transfer Coefficient (Assume  $P_X=0$ )

$$(k'_R)_1 = (P_{EI} + P_H + P_{gas} - P_{calor})/f(T)$$

True Heat Transfer Coefficient (Assume  $P_X$  is Constant)

$$(k'_R)_2 = (P_{EI} + P_H + P_X + P_{gas} - P_{calor})/f(T)$$

$$P_X = [(k'_R)_2 - (k'_R)_1]f(T)$$



# THEORETICAL RADIATIVE HEAT TRANSFER COEFFICIENT

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## Stefan-Boltzmann Coefficient

$$k_B = 5.6703 \times 10^{-12} \text{ Wcm}^{-2}\text{K}^{-4}$$

## Radiant Surface Area of Cell

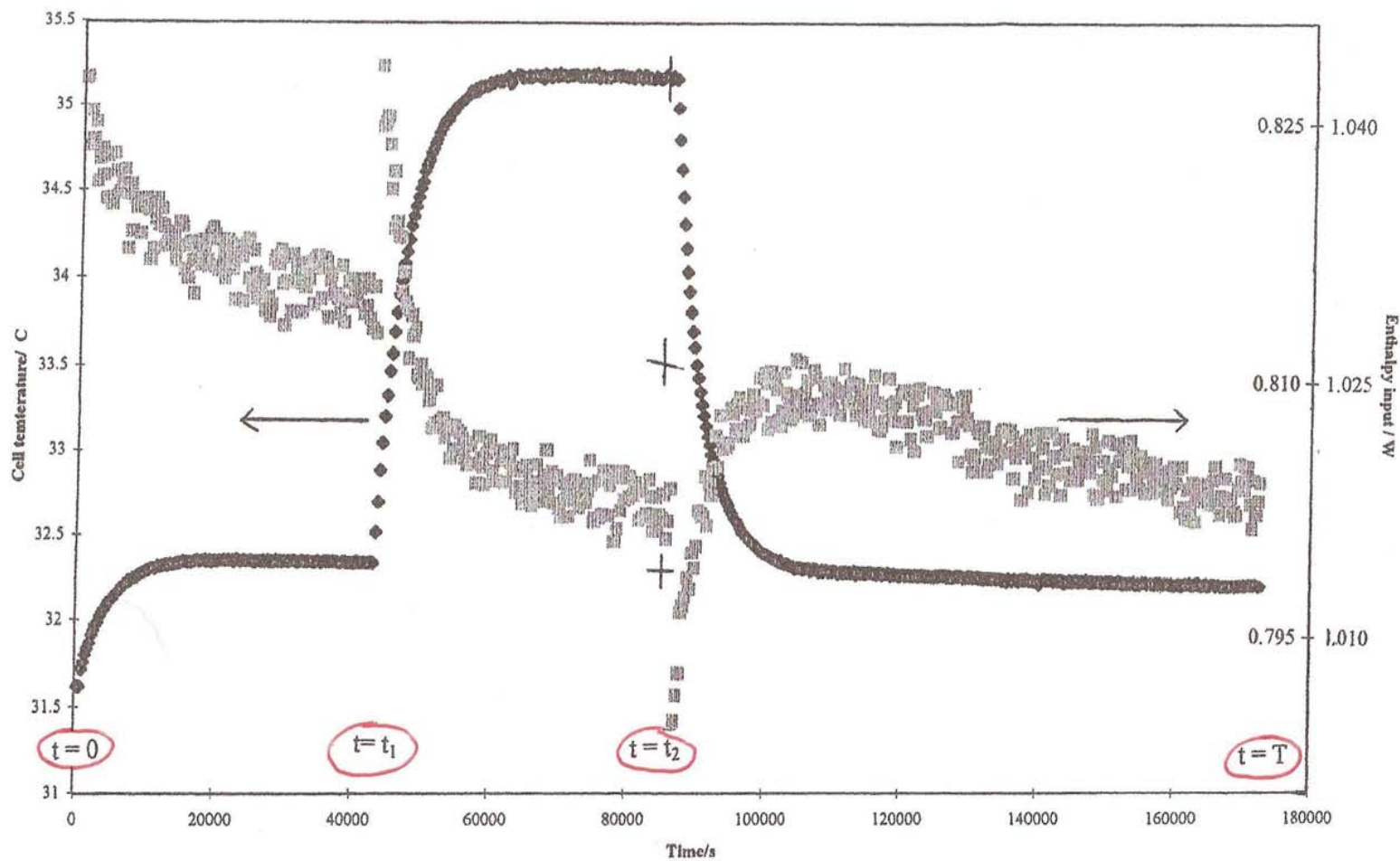
$$A = 109.7 \text{ cm}^2$$

## Theoretical Radiative Heat Transfer Coefficient

$$k_R = k_B A = (5.6703 \times 10^{-12} \text{ Wcm}^{-2}\text{K}^{-4})(109.7 \text{ cm}^2)$$

$$k_R = 0.622 \times 10^{-9} \text{ WK}^{-4}$$

# RAW DATA FOR DAYS 9 AND 10 ( $I = 0.200$ A)



## EVALUATION OF $(k'_R)^2$ AT $t=t_2$

$$(k'_R)_2 f(T)(t_2) = (P_{EI} + P_H + P_X + P_{gas} - P_{calor})(t_2) \quad (1)$$

$$(k'_R)_2 f(T)(t'_2) = (P_{EI} + P_X + P_{gas} - P_{calor})(t'_2) \quad (2)$$

Assume  $P_X$  is constant

(1) – (2) yields

$$\begin{aligned} (k'_R)_2 f_2(T) = & [P_{EI}(t_2) - P_{EI}(t'_2)] + P_H \\ & + [P_{gas}(t_2) - P_{gas}(t'_2)] \\ & - [P_{calor}(t_2) - P_{calor}(t'_2)] \end{aligned}$$

where

$$f_2(T) = (T_{cell}^4)t_2 - (T_{cell}^4)t'_2$$

# STRAIGHT LINE FORM

## ( $Y = a + bX$ )

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$$(P_{EI} + P_H + P_X + P_{gas})/f(T) = (k'_R)_2 + C_p M (dT_{cell}/dt)/f(T)$$

$$\text{Intercept} = (k'_R)_2$$

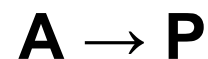
$$\text{Slope} = C_p M$$

$$f(T) = T_{cell}^4 - T_b^4$$

# CHEMICAL KINETICS ANALOGY

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## First Order Rate Law



### Differential Equation

$$-dA / dt = kA$$

### Integrated Rate Law

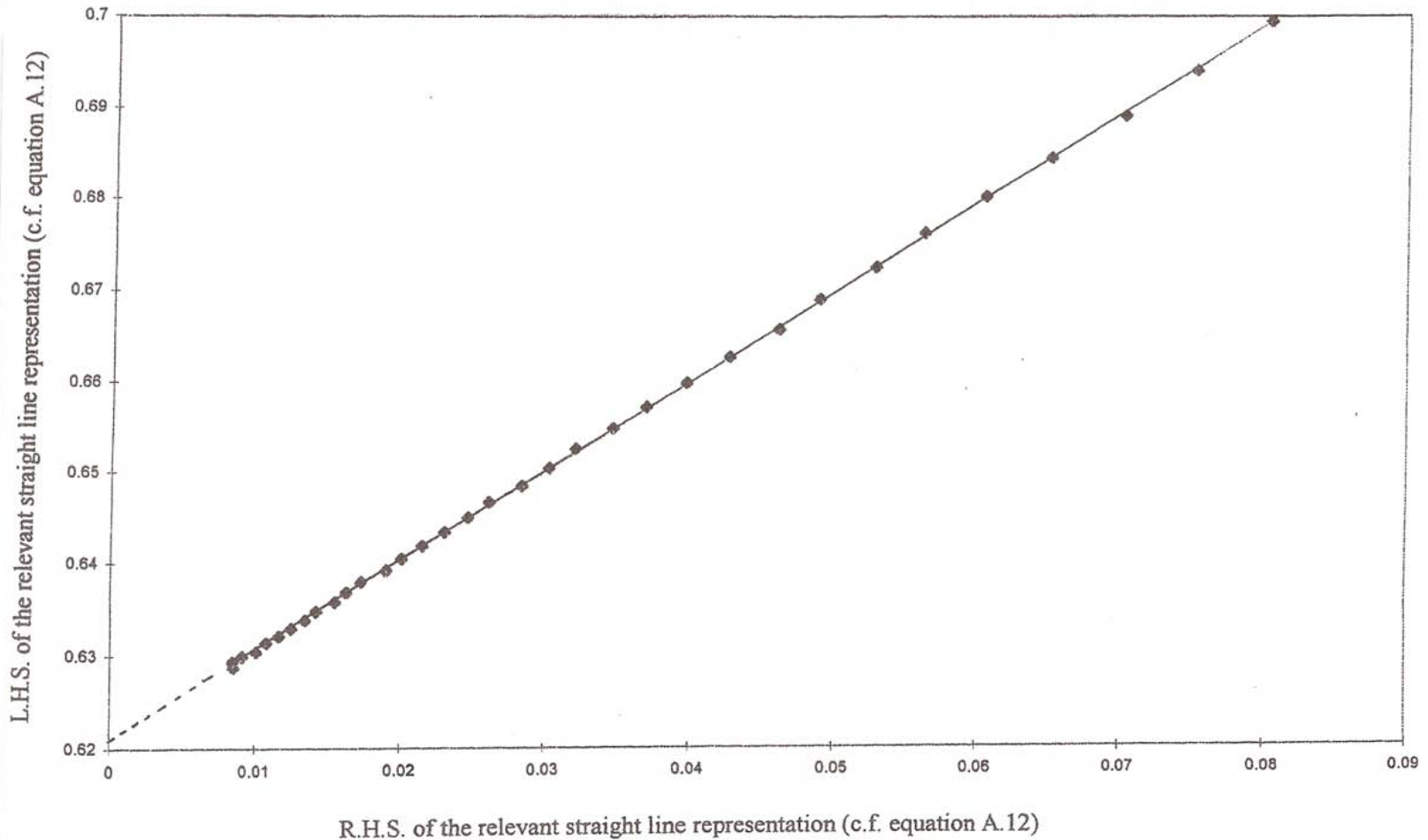
$$\ln A = \ln A_0 - kt$$

$$(y = a + bx)$$

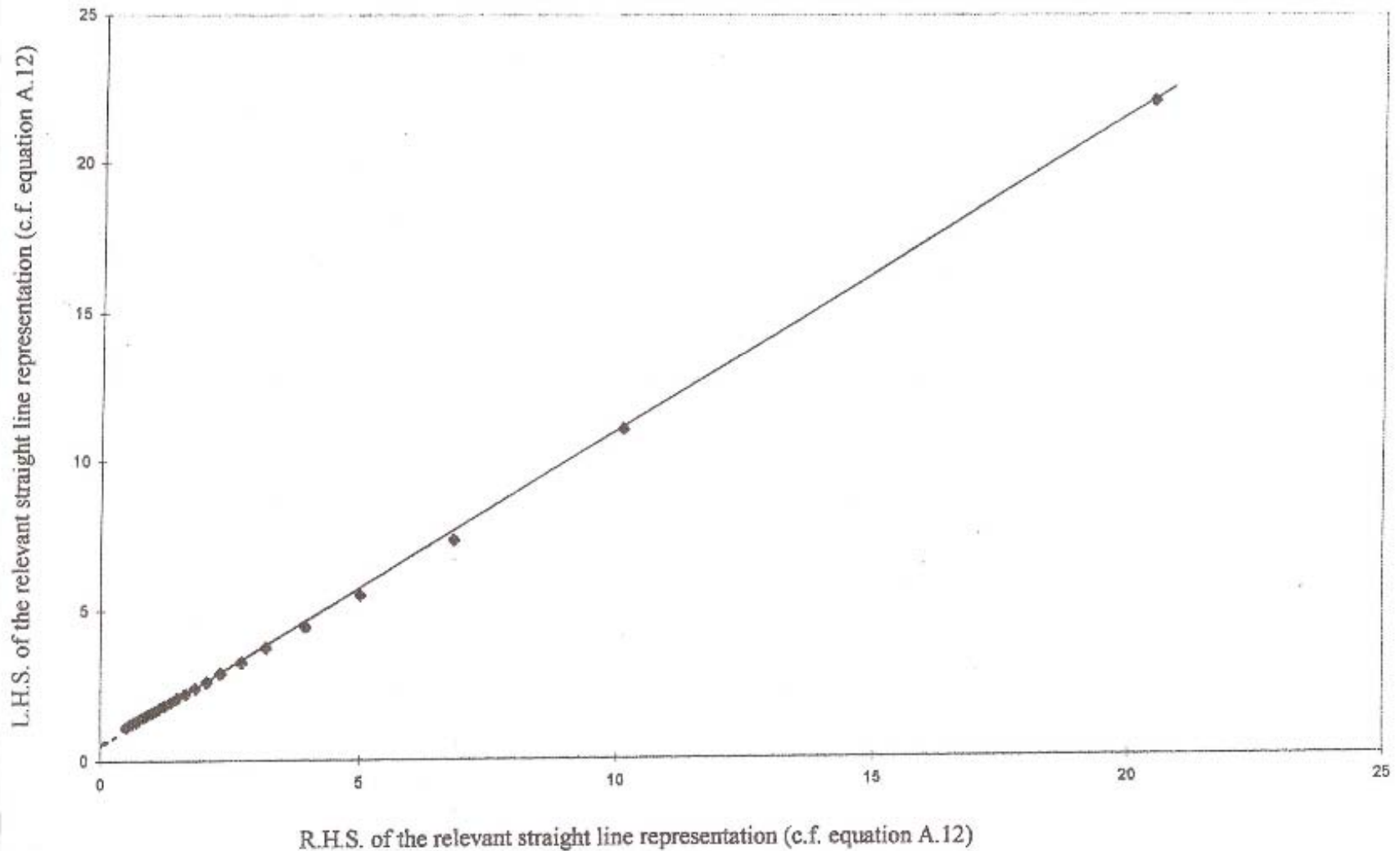
$$\text{slope} = -k$$

$$\text{Intercept} = \ln A_0$$

# EVALUATION OF $(k'_R)_{262}$ AND $C_pM$ (Backward Integration)



# EVALUATION OF $(k'_R)_{362}$ AND $C_p M$ (Forward Integration)

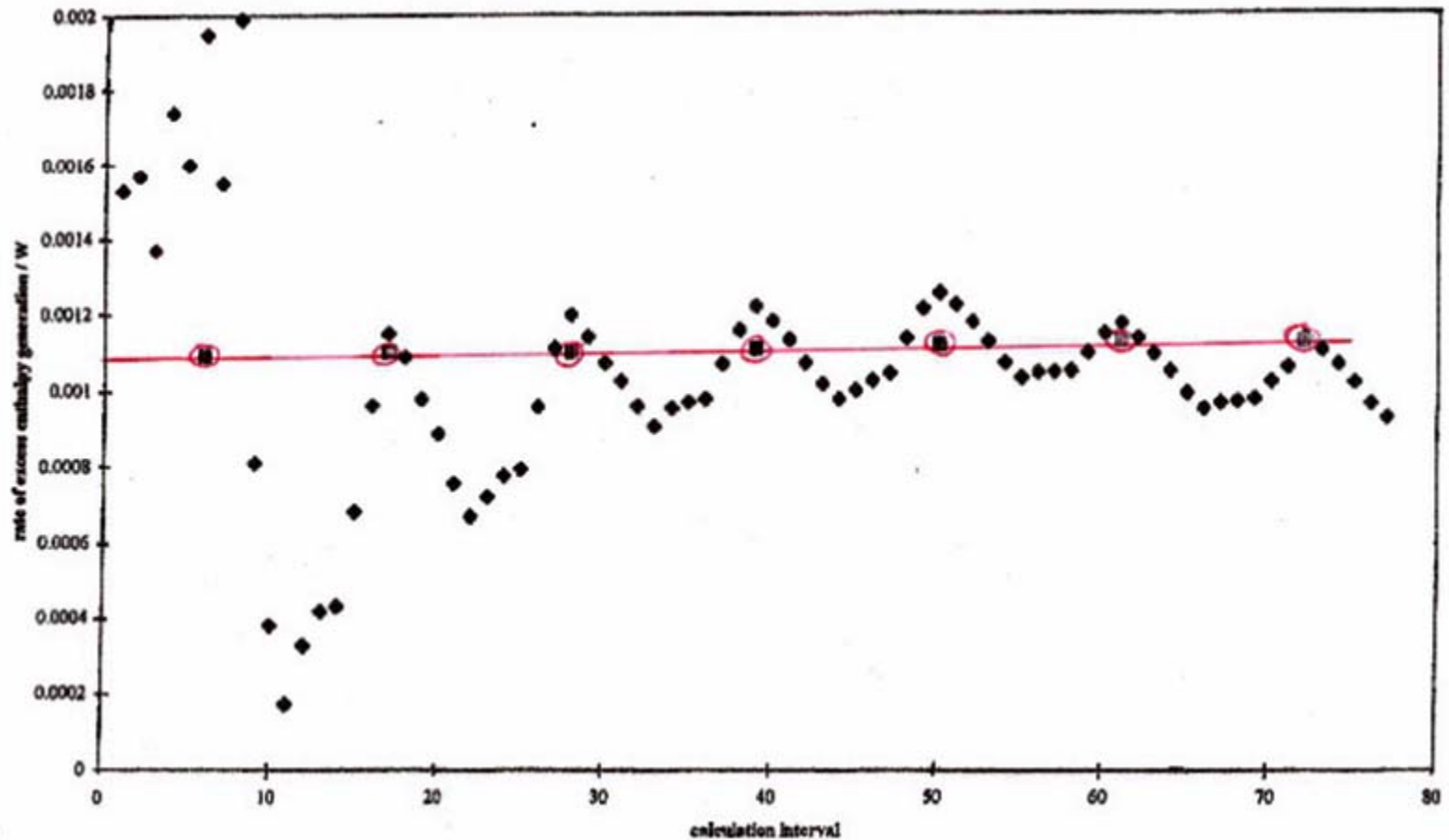




# MEAN VALUES FOR K AND C<sub>p</sub>M

<u>Description</u>	<u>10<sup>9</sup>(k'<sub>R</sub>), WK<sup>-4</sup></u>	<u>C<sub>p</sub>M, JK<sup>-1</sup></u>
Theoretical	0.622	340
(k' <sub>R</sub> ) <sub>1</sub> (lower bound)	0.62013 ±0.00058	-----
(k' <sub>R</sub> ) <sub>2</sub> (true)	0.62059 ±0.00240	-----
(k' <sub>R</sub> ) <sub>262</sub> <sup>0</sup> (backward Integration, True)	0.62083 ±0.00059	339.2 ±1.7
(k' <sub>R</sub> ) <sub>362</sub> <sup>0</sup> (forward Integration, True)	0.62031 ±0.00156	339.8 ±18.3

# Excess Power Due to Oxygen Reduction (Differential / Integral)



# THEORETICAL RATE OF OXYGEN REDUCTION EXCESS POWER

Henry's Law  $[O_2] = 1.2 \times 10^{-3} M = 1.2 \times 10^{-6} \text{ mol/cm}^3$

Fick's Law of Diffusion

$$I_L = DnF[O_2] A_E/\delta = 0.001 A$$

$$\text{where } D = 6 \times 10^{-6} \text{ cm}^2/\text{s} \quad A_E = 0.63 \text{ cm}^2$$

$$n = 4 \text{ eq/mol} \quad \delta = 0.002 \text{ cm}$$

Excess Power Due to Oxygen Reduction

$$P_X = E_H I_L = (1.527 \text{ V}) (0.001 \text{ A}) = 1.5 \text{ mW}$$

$$\text{for } \delta = 0.01 \text{ cm } I_L = 0.0002 \text{ A, } P_X = 0.3 \text{ mW}$$

$$\text{for } \delta = 0.001 \text{ cm, } I_L = 0.002 \text{ A, } P_X = 3.0 \text{ mW}$$

# PALLADIUM-BORON MATERIAL

PREPARED BY DR. M.A. IMAM, NAVAL RESEARCH LABORATORY

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Excess heat produced in 7 out of 8 experiments at China Lake

Excess heat produced in NHE (Japan) experiment

Materials contained 0.25 to 0.75 weight % boron

**Boron removes oxygen contamination in palladium**

Boron hardens palladium material

Boron resides in grain boundaries of palladium

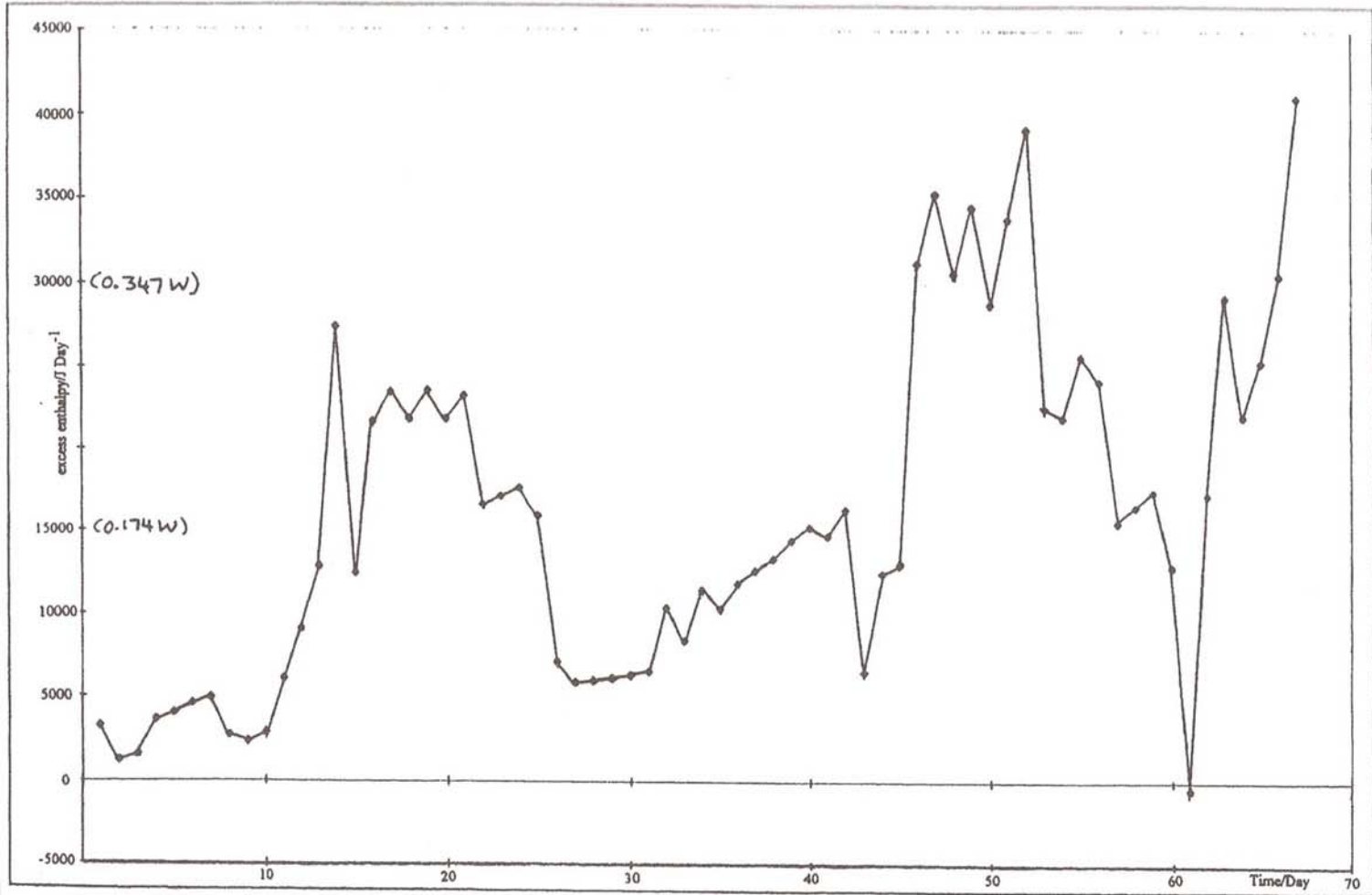
## U.S. Patent

**“Palladium-Boron Alloys for Excess Enthalpy Production”**

M.H. Miles and M. Ashraf Imam

U.S. Patent No. 6,764,561, June 20, 2004

# Pd-B RESULTS NHE/JAPAN



# CALORIMETRIC EQUATIONS AND CALCULATIONS (Further Information)

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## SEE:

1. Miles, M.H., Fleischmann, M. and Imam, M.A. (2001). Naval Research Laboratory Report Number NRL/MR/6320-01-8526, March 26, 2001.
2. Szpak, S. and Mosier-Boss, P.A. (2002). SPAWAR Systems Center Technical Report Number 1862, Volume 2, San Diego, CA.
3. Fleischmann, M. and Miles, M.H. (2006). In “Condensed Matter Nuclear Science”, pp. 247-268, P.L. Hagelstein and S.R. Chubb, Editors, World Scientific, New Jersey, ISBN No. 981-256-564-7.
4. Fleischmann, M. and Miles M.H. (2006). Manuscript No. JP058292J submitted to *J. Phys. Chem.* Note: Editor George C. Schatz rejected this manuscript and ruled that the two reviewers did not need to respond to the detailed rebuttal by the authors to the reviewers comments.

# SUMMARY

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- **Correct Equations Yield High Calorimetric Accuracy**
- **Backward Integration of Data Sets Yields Best Results**
- **Excess Power Measurable to  $\pm 0.1$  mW**
- **Reduction of Oxygen Measurable at 1.1 mW in Pt/D<sub>2</sub>O system**
- **Recombination Effects are Very Small (1.1 mW)**
- **Pd-B Material Yields Large Excess Power Effects (50 to 500 mW)**



# FURTHER INFORMATION / QUESTIONS

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## Further Information

**See: “Condensed Matter Nuclear Science”,  
Proceedings of ICCF-10, P.J. Hagelstein and S.R.  
Chubb, Editors,  
World Scientific, New Jersey ISBN 981-256-564-7, 2006,  
pp. 247-268.**

**My website: <http://coldfusion-miles.com>**

## Questions

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