



(19) **United States**

(12) **Patent Application Publication**
IWAMURA et al.

(10) **Pub. No.: US 2009/0290674 A1**

(43) **Pub. Date: Nov. 26, 2009**

(54) **NUCLIDE TRANSMUTATION DEVICE AND
NUCLIDE TRANSMUTATION METHOD**

(30) **Foreign Application Priority Data**

Oct. 31, 2000 (JP) 2000-333640
Jul. 3, 2001 (JP) 2001-201875

(75) Inventors: **Yasuhiro IWAMURA**,
Yokohama-shi (JP); **Takehiko Itoh**,
Yokohama-shi (JP); **Mitsuru**
Sakano, Yokohama-shi (JP)

Publication Classification

(51) **Int. Cl.**
G21G 1/10 (2006.01)
(52) **U.S. Cl.** **376/199**
(57) **ABSTRACT**

Correspondence Address:
**OBLON, SPIVAK, MCCLELLAND MAIER &
NEUSTADT, L.L.P.**
1940 DUKE STREET
ALEXANDRIA, VA 22314 (US)

The present invention produces nuclide transmutation using a relatively small-scale device. The device 10 that produces nuclide transmutation comprises a structure body 11 that is substantially plate shaped and made of palladium (Pd) or palladium alloy, or another metal that absorbs hydrogen (for example, Ti) or an alloy thereof, and a material 14 that undergoes nuclide transmutation laminated on one surface 11A among the two surfaces of this structure body 11. The one surface 11A side of the structure body 11, for example, is made a region in which the pressure of the deuterium is high due to pressure or electrolysis and the like, and the other surface 11B side, for example, is a region in which the pressure of the deuterium is low due to vacuum exhausting and the like, and thereby, a flow of deuterium in the structure body 11 is produced, and nuclide transmutation is carried out by a reaction between the deuterium and the material 14 that undergoes nuclide transmutation.

(73) Assignee: **MITSUBISHI HEAVY
INDUSTRIES, LTD.**, Tokyo (JP)

(21) Appl. No.: **12/483,827**

(22) Filed: **Jun. 12, 2009**

Related U.S. Application Data

(63) Continuation of application No. 09/981,983, filed on Oct. 19, 2001, now abandoned.

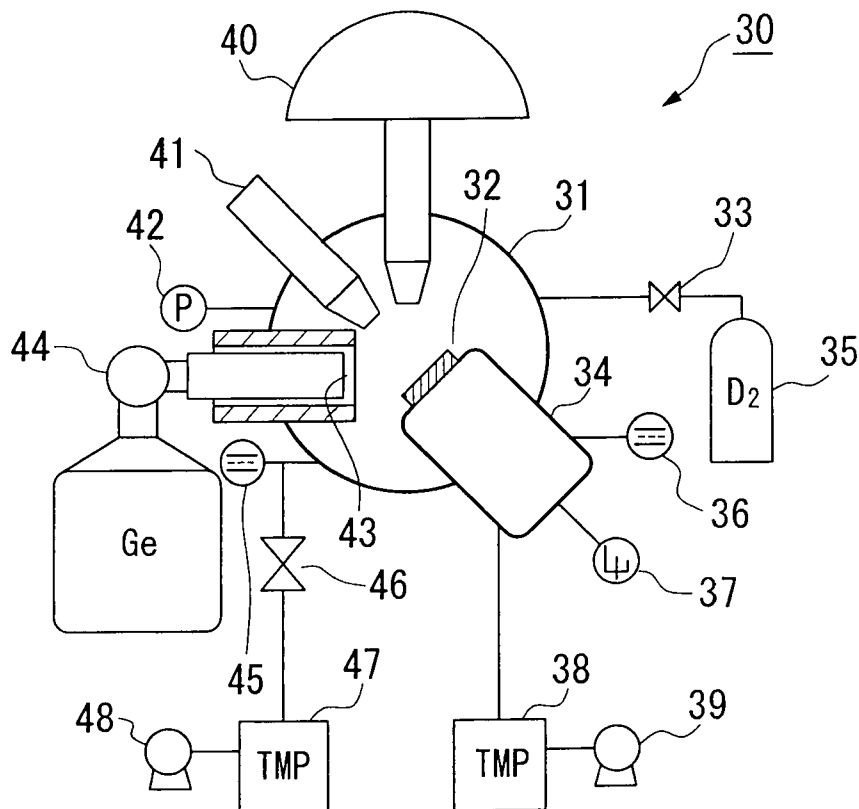


FIG. 1

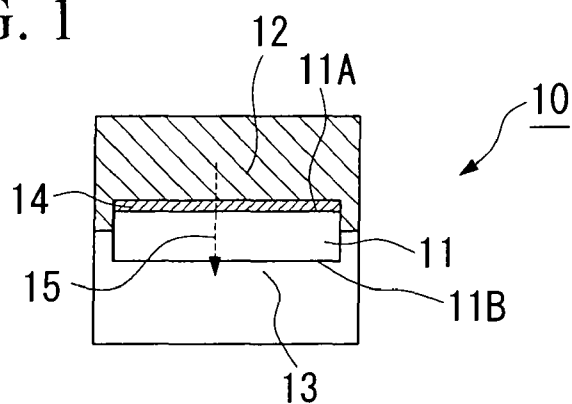


FIG. 2

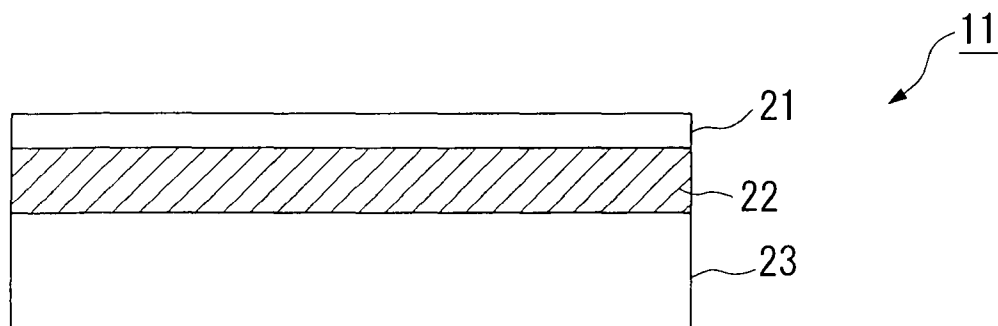


FIG. 3

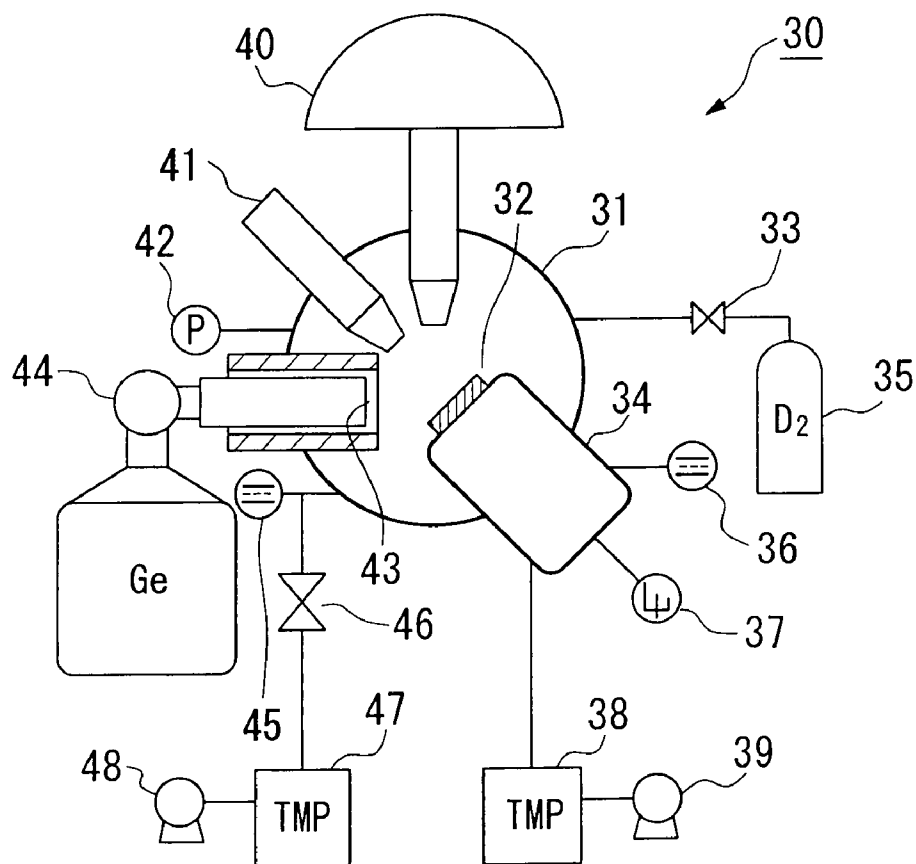


FIG. 4

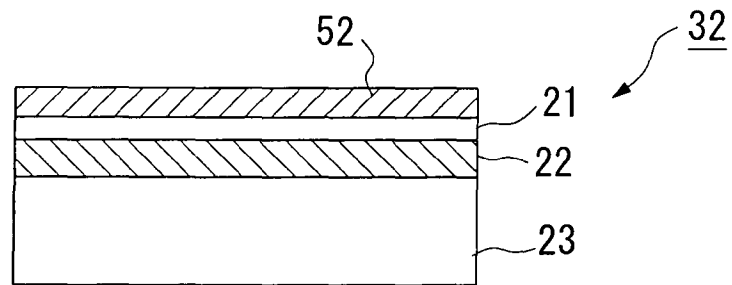


FIG. 5A

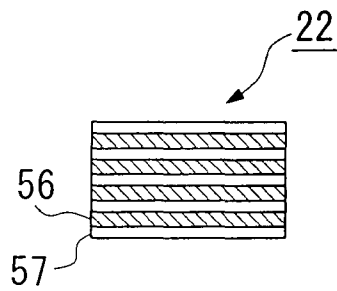


FIG. 5B

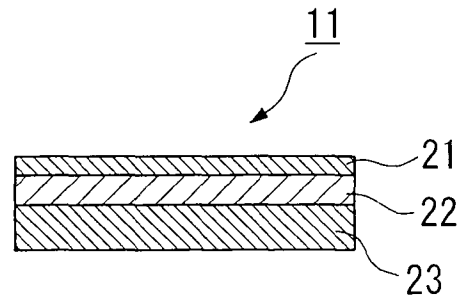


FIG. 6

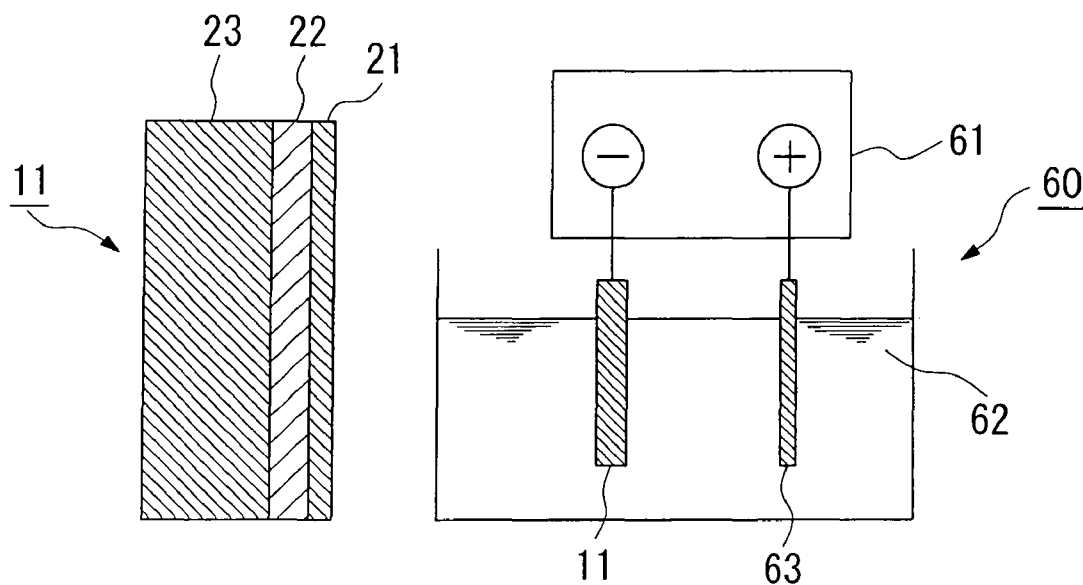


FIG. 7

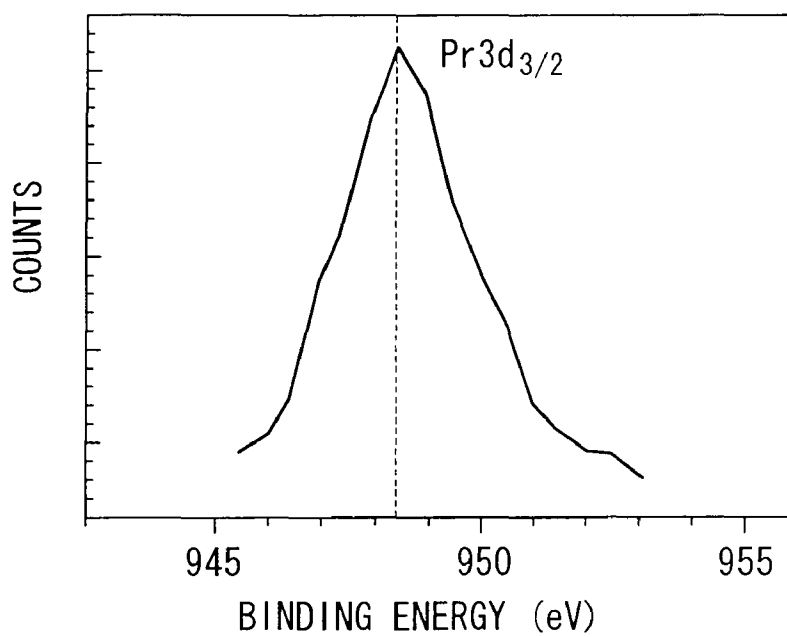


FIG. 8

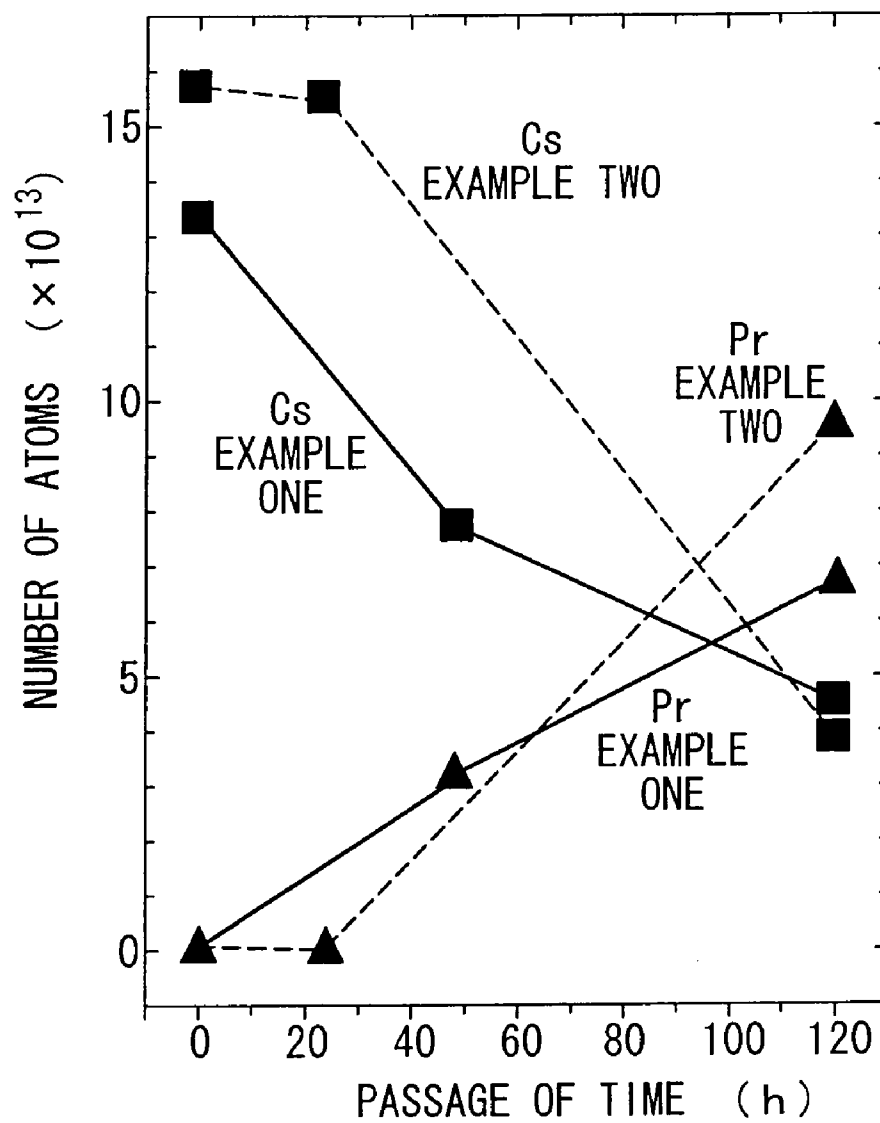


FIG. 9

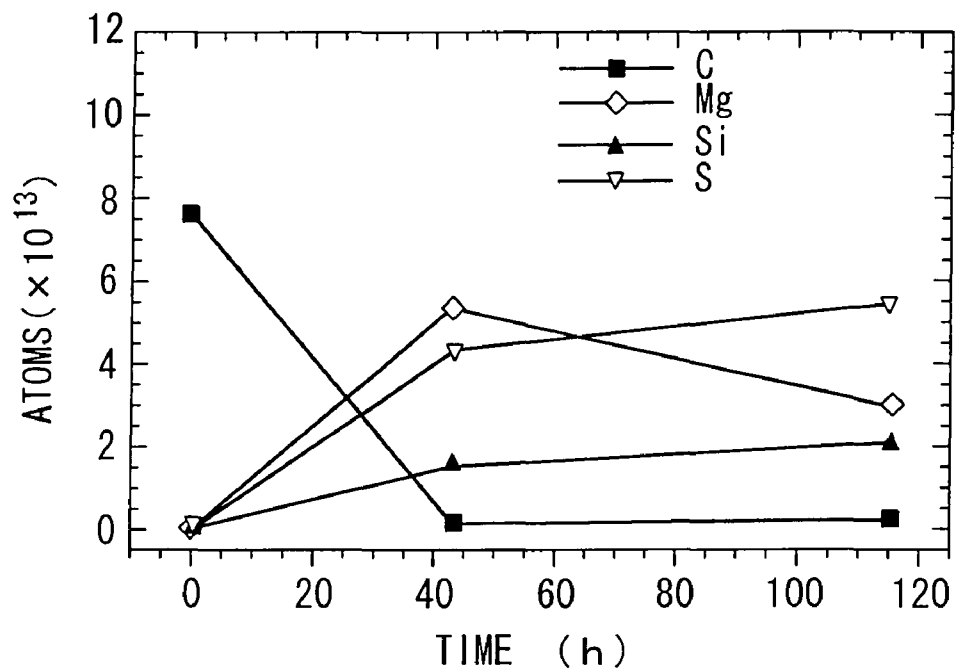


FIG. 10

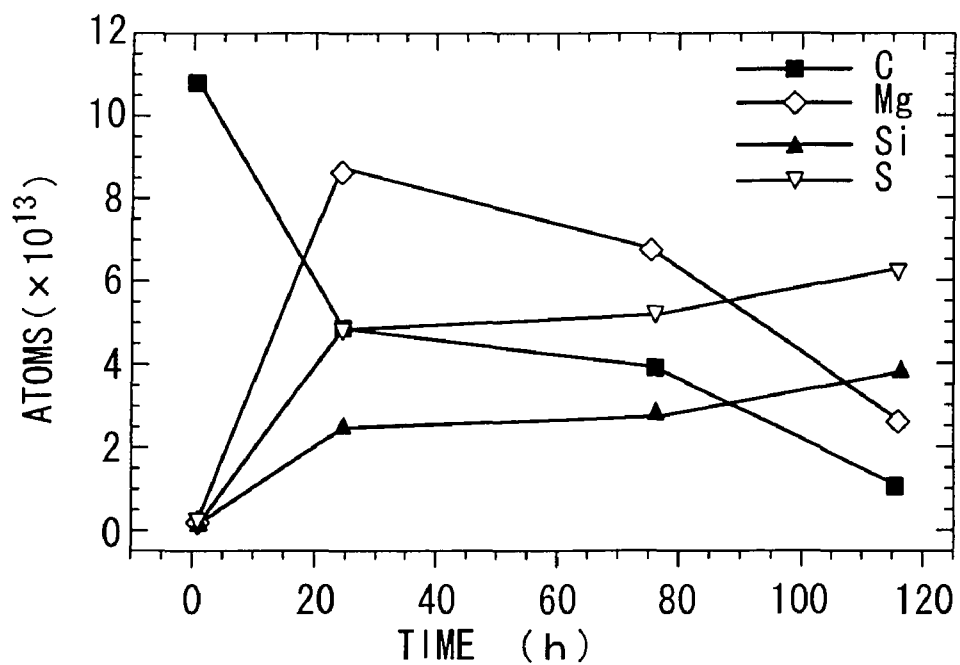


FIG. 11

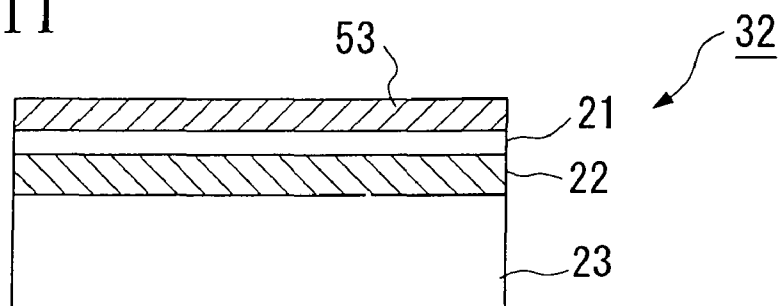


FIG. 12

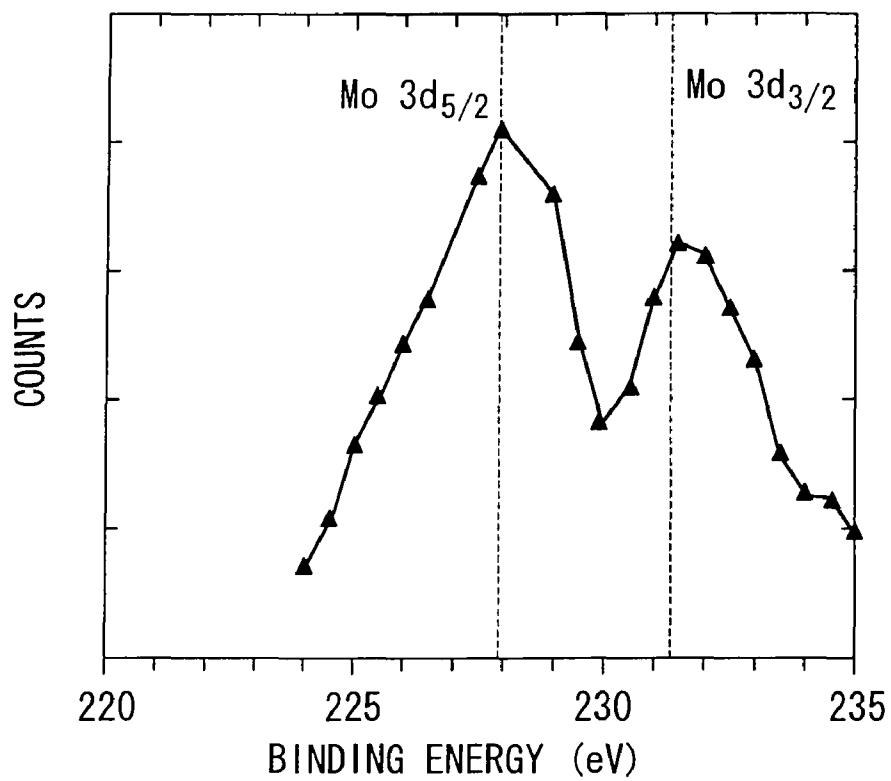


FIG. 13

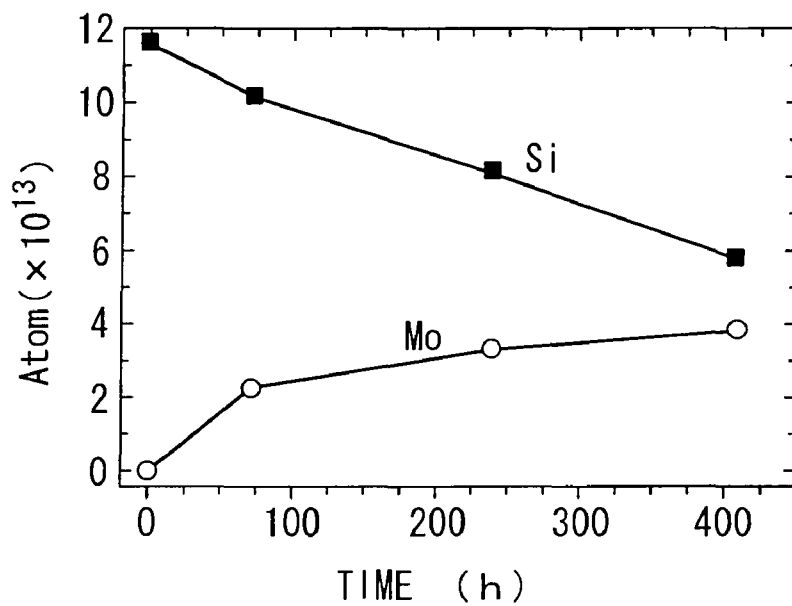


FIG. 14

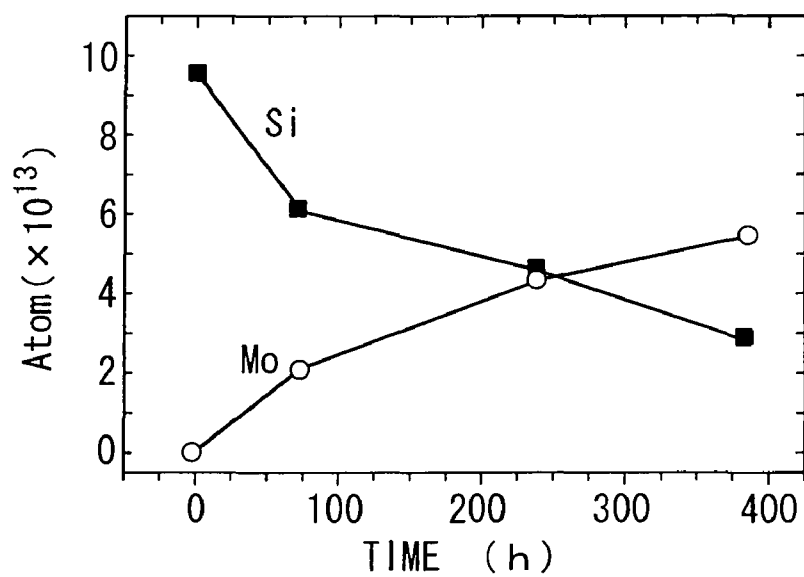


FIG. 15

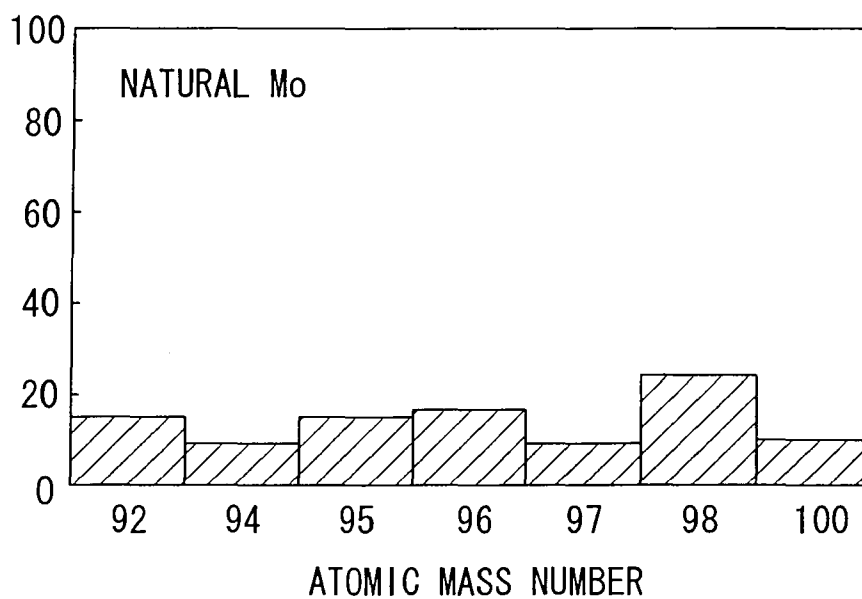


FIG. 16

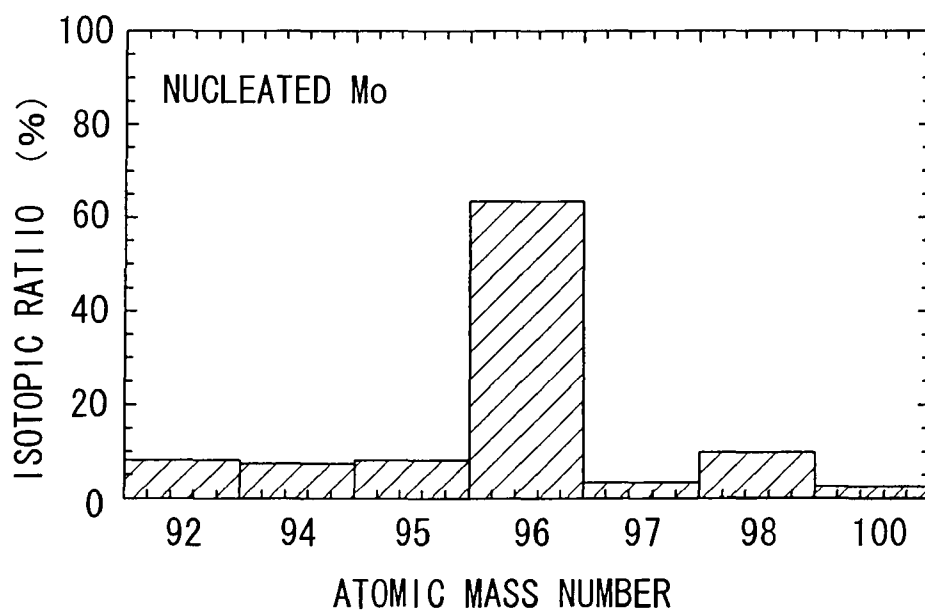


FIG. 17

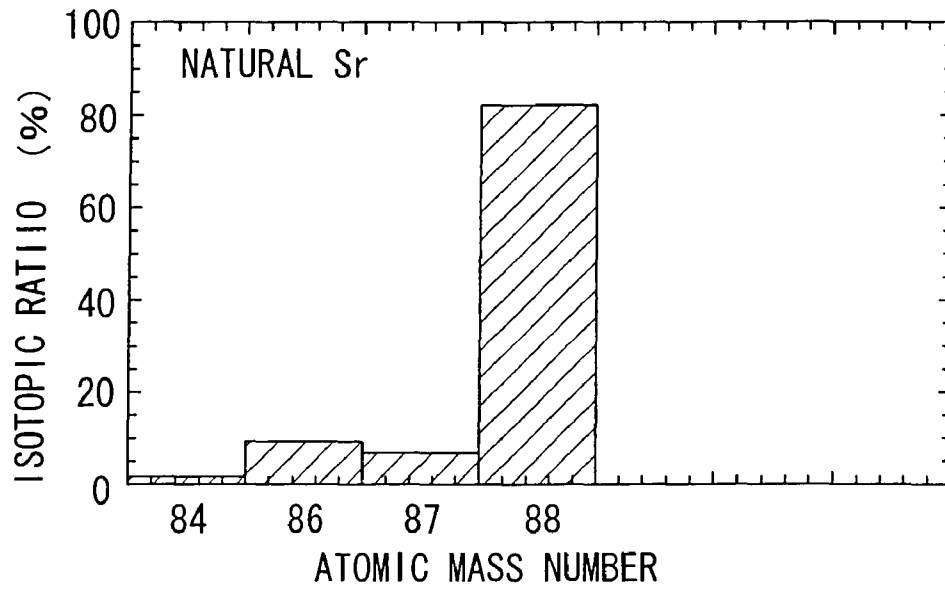


FIG. 18

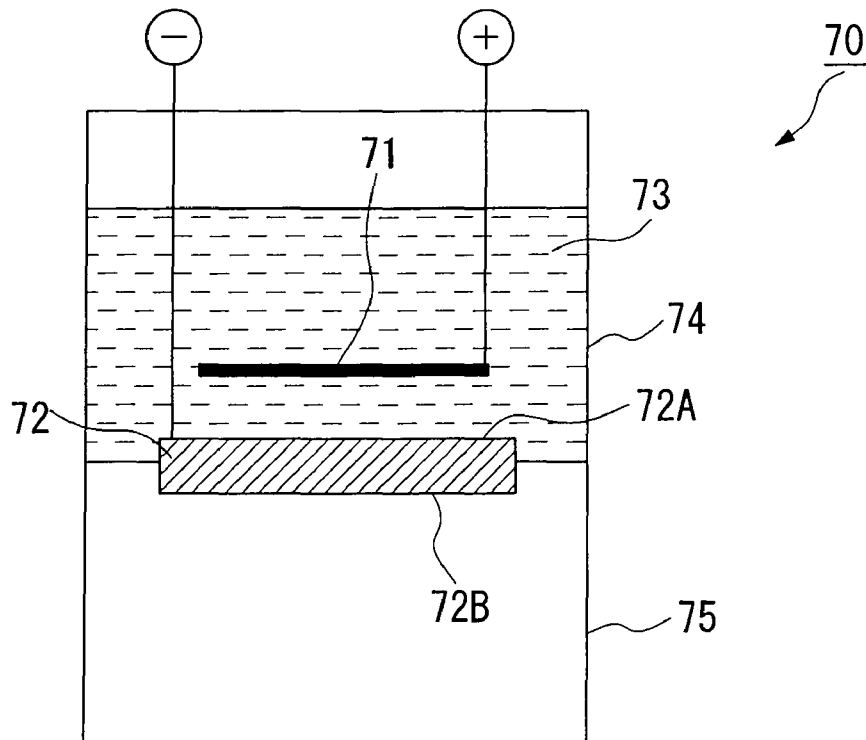


FIG. 19

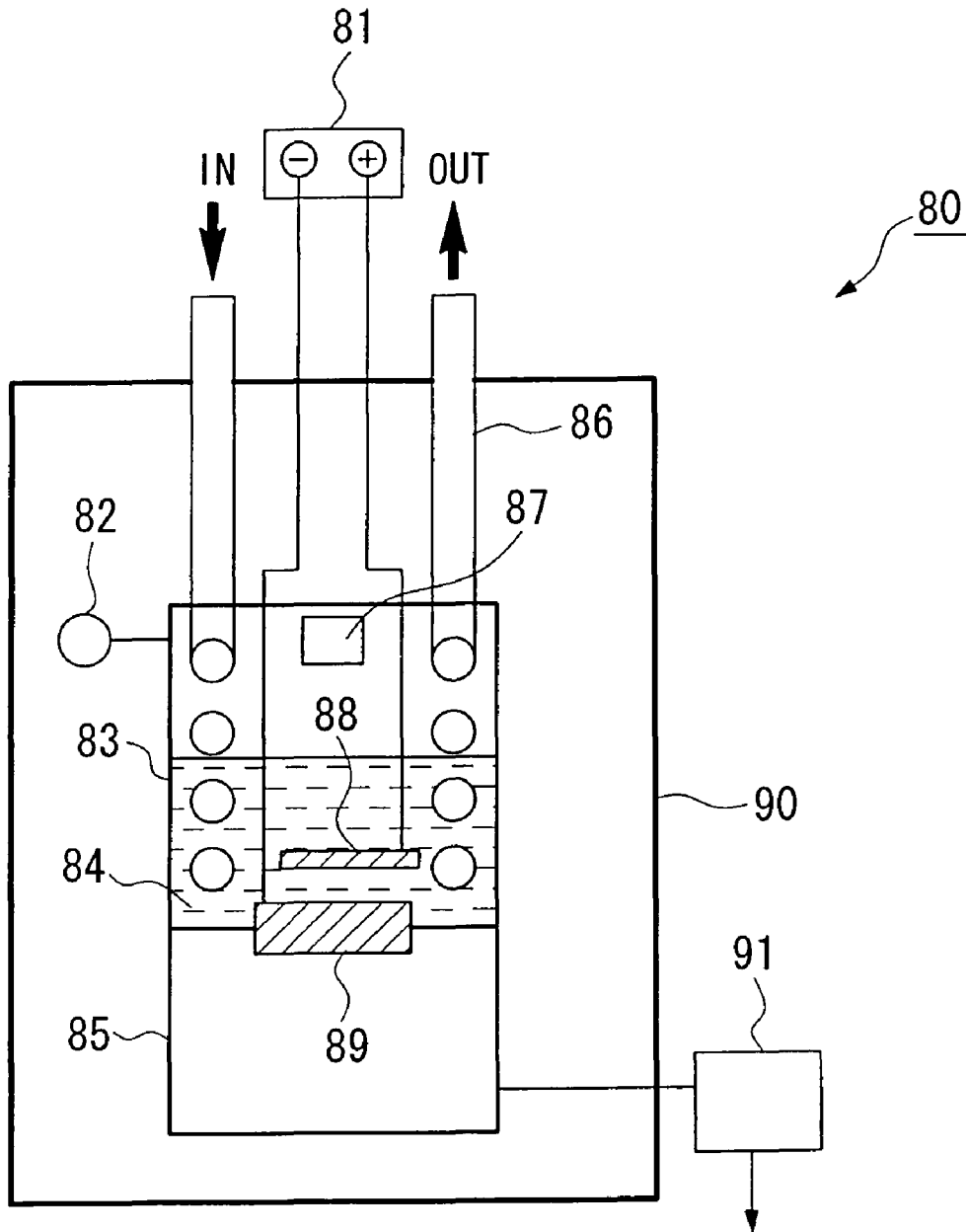


FIG. 20

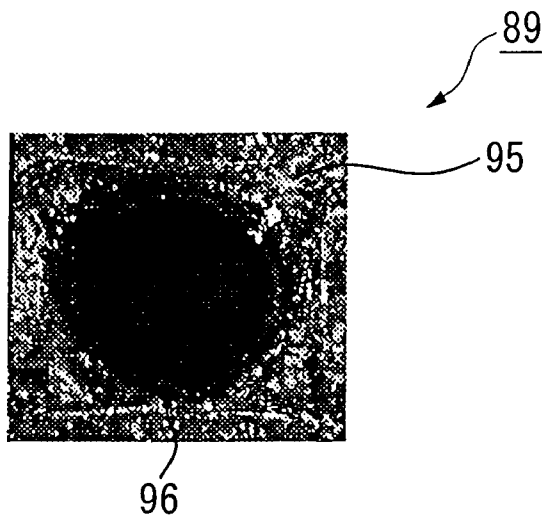


FIG. 21

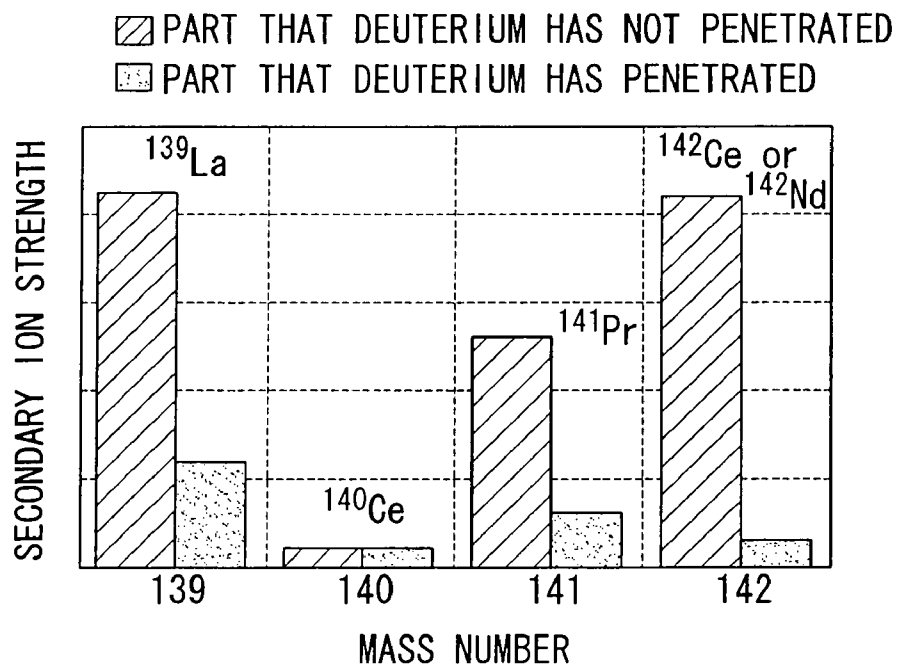
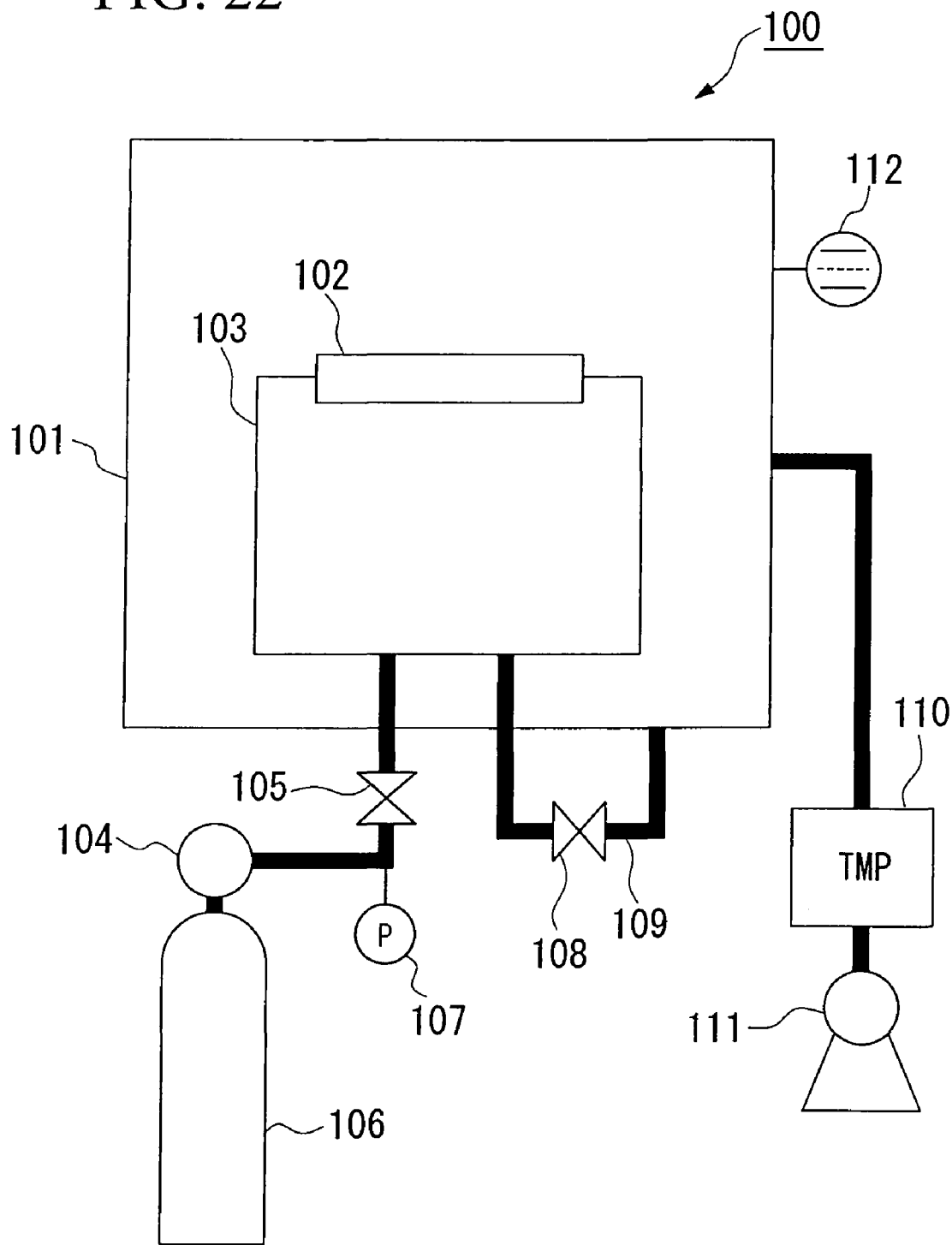


FIG. 22



NUCLIDE TRANSMUTATION DEVICE AND NUCLIDE TRANSMUTATION METHOD

CROSS REFERENCES TO RELATED APPLICATIONS

[0001] This application is a Continuation of and claims the benefit of priority under 35 U.S.C. §120 from U.S. Ser. No. 09/981,983, filed Oct. 19, 2001 the entire contents of which are incorporated herein by reference. U.S. Ser. No. 09/981,983, filed Oct. 19, 2001 claims the benefit of priority under 35 U.S.C. § 119 from Japanese Patent Application Nos. P2000-333640 filed Mar. 10, 2000 and P2001-201875 filed Mar. 7, 2001.

BACKGROUND OF THE INVENTION

[0002] 1. Field of the Invention

[0003] The present invention relates to a nuclide transmutation device and a nuclide transmutation method associated, for example, with disposal processes in which long-lived radioactive waste is transmuted into short-lived radioactive nuclides or stable nuclides, and technologies that generate rare earth elements from abundant elements found in the natural world.

[0004] 2. Description of the Related Art

[0005] Conventional disposal processes are known that include, for example, methods in which large amounts of long-lived radioactive nuclides included in high level radioactive waste and the like are efficiently and effectively transmuted in a short time. Examples of these methods are those in which small amounts of nuclide are transmuted, such as heavy element synthesis by a nuclear fusion reaction using a heavy ion accelerator.

[0006] These disposal processes are nuclide transmutation processes in which minor actinides such as Np, Am, and Cm included in high level radioactive waste, long-lived radioactive products of nuclear fission such as Tc-99 and I-129, exothermic Sr-90 and Cs-137, and useful platinum group elements such as Rh and Pd are separated depending on the properties of each of the elements (group separation), and subsequently causing a nuclear reaction by desorption of neutrons, the minor actinides having a long half-life and nuclear fission products, and transmuted into short-lived radioactive or non-radioactive nuclides. In addition, the useful elements and the long-lived radioactive nuclides included in the high level radioactive waste are separated and recovered, effective use of the elements is implemented, and at the same time, long-lived radioactive nuclides are transmuted into short-lived radioactive or stable nuclides.

[0007] Three types of disposal processing methods are known: disposal processing for actinides and the like by neutron irradiation in a nuclear reactor such as a fast breeder reactor or an actinide burn reactor; nuclear spallation processing for actinides and the like by neutron irradiation in an accelerator, and disposal processing of cesium, strontium, and the like by gamma ray irradiation in an accelerator.

[0008] By neutron irradiation in a nuclear reactor, minor actinides, which have a large neutron interaction cross-section, can be rationally processed, and in particular, by irradiation with fast neutrons, transuranic elements, whose nuclear fission is difficult to cause, can be directly caused to undergo nuclear fission.

[0009] However, long-lived radioactive nuclear fission products are difficult to process by neutron irradiation in a

nuclear reactor and the like, and for example, for Sr-90, Cs-137 and the like, which have a small neutron interaction cross section, disposal processing using an accelerator is applied.

[0010] In a disposal process using an accelerator, because unlike a nuclear reactor they are operated subcritically, the safety in relation to criticality is superior, and there is the advantage that there is a large degree of design freedom, and proton accelerators and electron beam accelerators are used.

[0011] In disposal processing using a proton accelerator, a nuclear spallation reaction is used in which high energy protons at, for example, 500 MeV to 2 GeV, are irradiated to spall the target nucleus, and nuclide transmutation is caused directly by using the nuclear spallation reaction. In addition, a nuclear fission reaction is generated by injecting the plurality of neutrons generated along with spallation of the target nucleus into a subcritical blanket placed around the target nuclei, and a nuclide transmutation reaction is generated by a neutron capture interaction. Thereby, for example, transuranic elements such as neptunium and americium and long-lived radioactive nuclear fission products can be disposed of, and furthermore, the heat generated by the subcritical blanket can be recovered and used for power generation, and the power necessary to operate to the proton accelerator can be made self-sufficient.

[0012] In addition, in disposal processing using an electron accelerator, disposal processing of long-lived radioactive nuclear fission products such as strontium and cesium and the transuranic elements and the like can be carried out by using gamma radiation generated by the bremsstrahlung of the proton beam or a large resonance reaction such as a photonuclear reaction, for example, the (γ , N) reaction and the (γ , nuclear fission) reaction, using gamma radiation and the like generated by a reverse Compton scattering by combining, for example, an electron accumulating ring and an optical cavity.

[0013] However, in the case of carrying out nuclide transmutation using a nuclear reactor or an accelerator, as in the disposal processes in the above-described examples of conventional technology, there are the problems in that large-scale and high cost apparatuses must be used, and the cost required for the nuclide transmutation increases drastically.

[0014] Furthermore, in the case of processing, for example, Cs-137, which is a long-lived radioactive nuclide fission product, when transmutating Cs-137 radiated from an electron power generator of about one million KW to another nuclide using an accelerator, there are problems in that the necessary power reaches one million KW and a high strength and large current accelerator become necessary, and thus efficiency is low.

[0015] In addition, in contrast to a thermal neutron flux of about $1 \times 10^{14}/\text{cm}^2/\text{sec}$ in a nuclear reactor such as a light water reactor, the neutron flux necessary for nuclide transmutation of Cs-137, which has a small neutron interaction cross section, is about 1×10^7 - $1 \times 10^{18}/\text{cm}^2/\text{sec}$, and there is the problem in that the necessary neutron flux cannot be attained.

SUMMARY OF THE INVENTION

[0016] In consideration of the above-described circumstances, it is an object of the present invention to provide a nuclide transmutation device and a nuclide transformation method that can carry out nuclide transmutation with a relatively small-scale device compared to the large-scale devices such as accelerators and nuclear reactors.

[0017] In order to attain the object related to solving the problems described above, the nuclide transmutation device according to a first aspect of the invention comprises a structure body (the structure body 11, the multilayer structure body 32, the cathode 72, the multilayer structure body 89, the multilayer structure body 102 in the embodiments) that is made of palladium or a palladium alloy, or a hydrogen absorbing metal other than palladium, or a hydrogen absorbing alloy other than a palladium alloy, an absorbing part (the absorbing chamber 31, the absorbing chamber 103, or the electrolytic cell 83 in the embodiments) and a desorption part (the desorption chamber 34, the desorption part 101, or the vacuum container 85 in the embodiments) that are disposed so as to surround the structure body on the sides and form a closed space that can be sealed by the structure body, a high pressurization device (the deuterium tank 35, the deuterium tank 106, or the power source 81 in the embodiments) that makes the absorption part side on the side of the surface of the structure body have a state wherein the pressure of the deuterium is relatively high, a low pressurization device (the turbo-molecular pumps 38 and 110, the rotary pumps 39 and 111, and a vacuum exhaust pump 91 in the embodiments) that makes the desorption part side on the other side of the surface of the structure body have a state wherein the pressure of the deuterium is relatively low, and a transmutation material binding device (the step S22, the step S44, or the step S04a, in the embodiments) that binds the material that undergoes nuclide transmutation on one surface of the structure body material (^{133}Cs , ^{12}C , and ^{23}Na in the embodiments) that undergoes nuclide transmutation on the one of the surface of the structure body.

[0018] According to the nuclide transmutation device having the structure described above, a pressure differential in the deuterium between the one surface and the other surface of the structure body is provided in a state wherein the material that undergoes nuclide transmutation is bound to one of the surfaces of the structure body serving as a multilayer structure, and within the structure body a flux of deuterium from one surface side to the other surface side is produced, and thereby an easily reproducible nuclide transmutation reaction can be produced for the deuterium and the material that undergoes nuclide transmutation.

[0019] Furthermore, the nuclide transmutation device according to a second aspect of the present invention is characterized in comprising a high pressurization device that provides a deuterium supply means (the deuterium tanks 35 and 106 in the embodiments) that supplies deuterium gas to the absorption part, and the low pressurization device provides an exhaust means (the turbo-molecular pumps 38 and 110, and the rotary pumps 39 and 111 in the embodiments) that brings about a vacuum state in the desorption part.

[0020] According to the nuclide transmutation device having the structure described above, the absorption part is pressurized by the deuterium supply device, and at the same time, the pressure in the radiation part is reduced to a vacuum state by the exhaust means, and thus a pressure differential in the deuterium is formed in the structure body.

[0021] Furthermore, the nuclide transmutation device according to a third aspect is characterized in the high pressurization device providing an electrolysis device (the power source 81 in the embodiments) that supplies an electrolytic solution (the electrolytic solution 84 in the embodiments) that includes deuterium to the absorption part and electrolyzes the electrolytic solution with the structure body serving as the

cathode, and the lower pressurization device provides an exhaust device (the vacuum exhaust pump 91 in the embodiments) that brings about a vacuum state in the radiation part.

[0022] According to the nuclide transmutation device having the structure described above, by electrolyzing the electrolytic solution on one surface of the structure body with the structure body serving as a cathode, deuterium is absorbed effectively into the structure body due to the high pressure, and by reducing the pressure of the radiation part to a vacuum state using the exhaust device, a pressure differential in the deuterium is formed in the structure body.

[0023] Furthermore, the nuclide transmutation device according to a fourth aspect of the present invention is characterized in the transmutation material binding device providing a transmutation material lamination device (step S04, step S44, or step S04a, in the embodiments) that laminates the material that undergoes nuclide transmutation onto one surface of the structure body.

[0024] According to the nuclide transmutation device having the structure described above, the transmutation material lamination means can laminate the material that undergoes the nuclear transmutation on one surface of the structure body by a surface forming process, such as electrodeposition, vapor deposition, or sputtering.

[0025] Furthermore, the nuclide transmutation device according to a fifth aspect of the present invention is characterized in the transmutation material binding device providing a transmutation material supply means (step S22 in the embodiments) that supplies a material that undergoes nuclide transmutation in the absorption part, and exposing one surface of the structure body to a gas or liquid that includes the material that undergoes the nuclide transmutation.

[0026] According to the nuclide transmutation device having the structure described above, the material that undergoes nuclide transmutation can be bound to one surface of the structure body by mixing the material that undergoes nuclide transmutation in, for example, a gas or liquid that includes deuterium.

[0027] Furthermore, the nuclide transmutation device according to the sixth aspect of the present invention is characterized in that the structure body provides from one surface to the other surface in order a base material (the Pd substrate 23 in the embodiments) that is made of palladium or a palladium alloy, or a hydrogen absorbing metal other than palladium, or a hydrogen absorbing alloy other than a palladium alloy; a mixed layer (the mixed layer 22 in the embodiments) that is formed on the surface of the base material and comprises palladium or a palladium alloy, or a hydrogen absorbing metal other than palladium or a hydrogen absorbing alloy other than a palladium alloy, and a material having a low work function (CaO in the embodiments); and a surface layer (the Pd layer 21 in the embodiments) that is formed on the surface of the mixed layer and comprises palladium or a palladium alloy, or a hydrogen absorbing metal other than palladium or a hydrogen absorbing alloy other than a palladium alloy.

[0028] According to the nuclide transmutation device having the structure described above, a mixed layer that includes a material having a low work function is provided on the structure body that serves as the multilayer structure, and thereby the repeatability of the production of the nuclide transmutation reaction is improved.

[0029] According to the nuclide transmutation device having the structure described above, the production of the nuclide transmutation reaction can be further promoted by

transmuting the material that undergoes nuclide transmutation to a nuclide having a similar isotope ratio composition.

[0030] In addition, the nuclide transmutation method according to a seventh aspect of the present invention is characterized in including in the structure body (the structure body 11, the structure body 32, multilayer structure body 32, the cathode 72, the multilayer structure body 89, and multilayer structure body 102 in the embodiments) comprising palladium or a palladium alloy, or a hydrogen absorbing metal other than palladium, or a hydrogen absorbing alloy other than a palladium alloy, a high pressurizing process (step S07, step S25, or step S46 in the embodiments) that brings about a state in which the pressure of the deuterium is relatively high on one surface side of the structure body, a low pressurizing process (step S05, step S23, or step S45 in the embodiments) that brings about a state in which the pressure of the deuterium is relatively low on the other surface side of the structure body, and a transmutation material binding process (step S 04 and step S 22 or steps S44 and S04a in the embodiments) that binds the material that undergoes nuclide transmutation to the one surface of the structure body.

[0031] According to the nuclide transmutation method described above, a pressure differential in the deuterium is provided between the one surface side and the other surface side of the structure body in a state in which the material that undergoes nuclide transmutation is bound to the one surface of the structure body that serves as the multilayer structure, and a flux of deuterium from the one surface side to the other surface side in the structure body is produced, and thereby the nuclide transmutation reaction is produced with good repeatability for the deuterium and the material that undergoes nuclide transmutation.

[0032] Furthermore, a nuclide transmutation method according to the eighth aspect of the present invention is characterized in the transmutation material binding process including either a transmutation material lamination process (step S04, step S44, or step S04a in the embodiments) that laminates the material that undergoes nuclide transmutation on the one surface of the structure body, or a transmutation material supply process (step S22 in the embodiments) that exposes the one surface of the structure body to a gas or liquid that includes the material that undergoes nuclide transmutation.

[0033] According to the nuclide transmutation method described above, a material that undergoes nuclide transmutation is laminated on the one surface of the structure body by a film formation process using a transmutation material lamination process such as electrodeposition, vaporization deposition, or sputtering, or the material that undergoes nuclide transmutation is mixed with a gas or liquid that includes deuterium and the like, and thereby the material that undergoes the nuclide transmutation are disposed on the one surface of the structure body.

[0034] Furthermore, a nuclide transmutation method according to a ninth aspect of the present invention is characterized in the transmutation material binding process that binds the material that undergoes nuclide transmutation to the one surface of the structure body.

[0035] According to the nuclide transmutation method described above, the material that undergoes nuclide transmutation is transmuted to a nuclide having a similar isotopic ratio composition, and thereby the nuclide transmutation reaction can be promoted.

BRIEF DESCRIPTION OF THE DRAWINGS

[0036] FIG. 1 is a drawing for explaining the principle of the nuclide transmutation method according to the first embodiment of the present invention.

[0037] FIG. 2 is a cross-sectional structural drawing showing the structure body used in the nuclide transmutation method according to the first embodiment of the present invention.

[0038] FIG. 3 is a structural diagram of the nuclide transmutation device according to the first embodiment of the present invention.

[0039] FIG. 4 is a cross-sectional structure drawing of the multilayer structure body used in the nuclide transmutation device shown in FIG. 3.

[0040] FIG. 5A is a cross-sectional structural drawing of the mixed layers and FIG. 5B is a cross-sectional structural drawing of the structure body including the mixed layer.

[0041] FIG. 6 is a structural diagram of the device that adds a material to be subjected to the nuclide transmutation to the multilayer structure body.

[0042] FIG. 7 is a graph showing the spectra of Pr by XPS in on the surface of the multilayer structure body shown in FIG. 4.

[0043] FIG. 8 is a graph showing the change in the number of Cs and Pr atoms over time on the surface of the multilayer structure body shown in FIG. 5.

[0044] FIG. 9 is a graph showing the change in the number of atoms for each of C, Mg, Si, and S over time on the surface of the multilayer structure body in the third embodiment.

[0045] FIG. 10 is a graph showing the change in the number of atoms for each of C, Mg, Si, and S over time on the surface of the multilayer structure body in the fourth embodiment.

[0046] FIG. 11 is a cross-sectional structure showing a multilayer structure body according to the second modified embodiment of the present invention.

[0047] FIG. 12 is a graph showing an XPS spectrum of Mo on the surface of the multilayer structure body shown in FIG. 11.

[0048] FIG. 13 is a graph showing the change in the number of Sr and Mo atoms over time on the surface of the multilayer structure body shown in FIG. 11.

[0049] FIG. 14 is a graph showing the change in the number of Sr and Mo atoms over time on the multilayer structure body shown in FIG. 11.

[0050] FIG. 15 is a graph showing the change of the isotopic ratio of the natural Mo with the change of the atomic mass number over time.

[0051] FIG. 16 is a graph showing the change of the isotopic ratio of the nucleated Mo on the surface of the multilayer structure body according to the fifth embodiment of the present invention together with the change in its atomic mass number.

[0052] FIG. 17 is a diagram showing the change of the isotopic ratio of the natural Sr, which is added as a material that undergoes nuclide transmutation, together with the change in its mass number.

[0053] FIG. 18 is a diagram explaining the principle of the nuclide transmutation according to the second embodiment of the present invention.

[0054] FIG. 19 shows a structure of the nuclide transmutation device according to the second embodiment of the present invention.

[0055] FIG. 20 is a drawing showing the surface on the electrolyte cell side of the multilayer structure body after experiments using the nuclide transmutation device shown in FIG. 19.

[0056] FIG. 21 is a graph showing the results of SIMS analysis of the surface of the multilayer structure body after experiments using the nuclide transmutation device shown in FIG. 19.

[0057] FIG. 22 shows a structure of a nuclide transmutation device according to the third embodiment of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

[0058] Below, the nuclide transmutation device and nuclide transformation method according to the first embodiment of the present invention are explained referring to the figures.

[0059] FIG. 1 is a drawing for explaining the principle of the nuclide transmutation method according to the first embodiment of the present invention; FIG. 2 is a cross-sectional structural drawing showing the structure body 1 used in the nuclide transmutation method according to the first embodiment of the present invention; FIG. 3 is a structural diagram of the nuclide transmutation device 30 according to the first embodiment of the present invention; FIG. 4 is a cross-sectional structure drawing of the structure body 51 used in the nuclide transmutation device shown in FIG. 3; FIG. 5A is a cross-sectional structural drawing of a mixed layer 22 and FIG. 5B is a cross-sectional drawing of the structure body 11 containing the mixed layer 22; FIG. 6 is a diagram of the device that adds a material, that undergoes nuclide transmutation, to the structure body 11.

[0060] As shown, for example, in FIG. 1, the device 10 that realizes the nuclide transmutation method according to the present embodiment comprises a structure body 11 having a substantially plate shape comprising palladium (Pd) or an alloy of Pd or another metal (for example, Ti) that absorbs hydrogen, or an alloy thereof, and a material that undergoes nuclide transmutation attached to one surface 11A among the two the surfaces of this structure body 11; and in the device a flow 15 of deuterium is generated in the structure body 11 due to the one surface side 11A of the structure body 11 serving as a region 12 in which, for example, a load or the pressure of hydrogen due to electrolysis is high and the other surface 11B side serving as a region 13 in which the pressure of the deuterium due to vacuum exhaust and the like is low; and the nuclide transmutation is carried out by the reaction between the deuterium and the material 14 that undergoes nuclide transmutation.

[0061] Here, as shown for example in FIG. 2, the structure body 11 is preferably formed by a mixed layer 22 of a material that has a relatively low work function, that is, a material that emits electrons easily (for example, a material having a work function equal to or less than 3 eV), and Pd being formed on the surface of a Pd substrate 23, and a Pd layer 21 being laminated on surface of the mixed layer 22.

[0062] As shown in FIG. 3, the nuclide transmutation device 30 according to the present embodiment comprises an absorption chamber 31 having an interior that can be maintained in an airtight state, a radiation chamber 34 provided inside this absorption chamber 31 that can be maintained airtight due to the multilayer structure body 32, a deuterium tank 35 that supplies deuterium into the absorption chamber 31 via the variable leak pump 33, a radiation chamber vacuum gauge 36 that detects the degree of the vacuum in the radiation chamber 34, a substance analyzer 37 that detects the gaseous reaction products produced, for example, from the multilayer structure body 32, and evaluates the amount of penetration of the deuterium that penetrates the multilayer structure body 32

by measuring the amount of deuterium in the radiation chamber 34, a turbo-molecular pump 38 that always maintains the interior of the radiation chamber 34 in a vacuum state, and a rotary pump 39 for preliminary evacuating the radiation chamber 34 and the turbo-molecular pump 38.

[0063] Further, the nuclide transmutation device 30 comprises static electricity analyzer 40 that detects photoelectrons, ions, and the like emitted from the atoms of the surface of the multilayer structure body 32 that are excited due to irradiation by X-rays, an electron beam, and a particle beam and the like, an X-ray gun 41 for XPS (X-ray Photo-electron Spectrometry) that radiates X-rays on one surface exposed to deuterium among the two surfaces of the multilayer structure body 32 in the absorption chamber 31 that is exposed to deuterium, a pressure meter 42 that detects pressure in the absorption chamber 31 into which deuterium has been introduced, an X-ray detector comprising, for example, a high purity germanium detector 44 having a beryllium window 43, an absorption chamber vacuum meter 45 that detects the degree of the vacuum in the absorption chamber 31, a vacuum valve that maintains the interior of the absorption chamber 31 in a vacuum state 46 before the introduction of the deuterium, for example, a turbo-molecular pump 47 that evacuates the absorption chamber 31 to a vacuum state, and a rotary pump 48 for preliminary evacuating the absorption chamber 31 and the turbo-molecular pump 47.

[0064] In addition, by placing the absorption chamber 31 side of the multilayer structure body 32 in a condition in which the pressure of the deuterium is relatively high placing the radiation chamber 34 side of the multilayer body 32 in a condition in which the pressure of the deuterium is relatively low, and forming the pressure difference in the deuterium on both surfaces of the multilayer structure body 32, a flow of deuterium from the absorption chamber 31 side to the radiation chamber 34 side is produced.

[0065] Here, as shown in FIG. 4, for example, the multilayer structure body 32 is formed such that a mixed layer 22 of a material that has a relatively low work function (for example, a material having a work function equal to or less than 3 eV) and Pd is formed on the surface of the Pd substrate 23, the Pd layer 21 is laminated on the surface of this mixed layer 22, and a cesium (Cs) layer 5 is added to the surface of the Pd layer 21 as the material that undergoes nuclide transmutation.

[0066] The nuclide transmutation device 30 according to the present embodiment is provided, and next, the method for carrying out the nuclide transmutation using this nuclide transmutation device 30 will be explained referring to the figures.

[0067] First, the Pd substrate 23 (for example, having a length of 25 mm, a width of 25 mm, a depth of 0.1 mm, and a purity of 99.5% or greater) shown in FIG. 2, for example, is degreased by ultrasound cleaning over a predetermined time interval in acetone. In addition, in a vacuum (for example, equal to or less than 1.33×10^{-15} Pa), annealing, that is, heat processing, is carried out over a predetermined time interval at 900° C. (step S01).

[0068] Next, at room temperature, contaminants are removed from the surface of the Pd substrate 23 after annealing by carrying out etching processing over a predetermined time interval (for example, 100 seconds) using heavy aqua regia (step S02).

[0069] Next, using a sputtering method employing an argon ion beam, the structure body 11 is produced by carrying out

surface formation on the Pd substrate **23** after the etching processing. Here, for example, the thickness of the Pd layer **21** shown in FIG. 2 is 400×10^{-10} m, and the mixed layer **22** of the material having a low work function and the Pd, as shown in FIG. 5A, is formed by alternately laminating, for example, a CaO layer **57** having a thickness of 100×10^{-10} m and, or example, a Pd layer **56** having a thickness of 100×10^{-10} , and thus the thickness of the mixed layer **22** is 1000×100 . In addition, by forming as a film a Pd layer **21** on the surface of the mixed layer **22** of 400×10^{-10} , the structure body **11** is formed (step S03).

[0070] Next, by electrolysis of CsNO_3 of a dilute solution of D_2O (a solution of $\text{CsNO}_3/\text{D}_2\text{O}$), as an example that undergoes nuclide transmutation, for example, the material Cs is added to the film processed surface of the structure body **11**. For example, like the electrodeposition device **60** shown in FIG. 6 using 1 mM of a $\text{CsNO}_3/\text{D}_2\text{O}$ solution as the electrolyte **62**, connecting the platinum electrode **63** to the anode of the power source **61**, connecting the structure body **11** to the cathode, and carrying out electrolysis over a 10 second interval at a voltage of 1V, the reaction represented by the following chemical Formula (1) is produced, a Cs layer **52** is added, and the multilayer structure body **32** is formed (step S04).



[0071] In addition, the Cs layer **52** of the multilayer body **32** is faced towards the absorption chamber **31** side, the absorption chamber **31** and the desorption chamber **34** are closed into an airtight state by interposing the multilayer structure body **32**. The desorption chamber **34** is evacuated first using a rotary pump **39** and a turbo molecular pump **38**. Furthermore, the absorption chamber **31** is evacuated using the rotary pump **48** and the turbo molecular pump **47** by closing the variable leak valve **33** and by opening the vacuum valve **46** (step S05).

[0072] Next, after sufficiently stabilizing the degree of the vacuum of the absorption chamber **31** (for example, to be equal to or less than 1×10^{-15} Pa), the elements present on the surface of the multilayer structure body **32** on the absorption chamber **31** side are analyzed by XPS (step S06). That is, the surface of the multilayer structure body **32** is irradiated by an X-ray beam from an X-ray gun **41**, and energy of the photoelectrons emitted from atoms on the surface of the multilayer structure body **32** excited by the X-ray irradiation is analyzed by the electrostatic analyzer **40** so that the elements present on the absorption chamber **31** side surface of the multilayer structure body **32** are identified.

[0073] Next, after heating the multilayer structure body **32** by a heating device (not shown), for example, to 70°C ., the vacuum exhausting of the absorption chamber **31** is suspended by closing the vacuum valve **46**, a deuterium gas is introduced at a predetermined gas pressure into the absorption chamber **31** by opening the variable leak valve **33**, and the experiment on nuclide transmutation is commenced. Here, the gas pressure when deuterium is introduced into the absorption chamber **31** is, for example, 1.01325×10^5 Pa (or 1 atmosphere).

[0074] In addition, measurement of the gaseous reaction product (for example, the mass number $A=1$ to 140) is carried out using the mass spectrograph **37** in the radiation chamber **34**, and the diffusion behavior of the deuterium that penetrates through the multilayer structure body **32** and is radiated into the radiation chamber **34** is evaluated. In addition, measurement of the X-ray is carried out by a high purity germanium

detector **44** disposed on the absorption chamber **31** side of the multilayer structure body **32** (step S07).

[0075] Note that the amount of deuterium released into the desorption chamber **34** after permeating through the multilayer structure body **32** is calculated based on the degree of vacuum in the desorption chamber **34** detected by a desorption chamber vacuum gauge **36** and a volume flow rate of a turbo molecular pump **38**.

[0076] After the commencement of the introduction of the deuterium gas into the absorption chamber **31**, for example, after several tens of hours, the temperature of the multilayer structure body **32** is restored to room temperature. The introduction of the deuterium gas is suspended by closing the variable leak valve **33**, and furthermore, the absorption chamber **31** is evacuated by opening the vacuum valve **46** and the experiment on nuclide transmutation is ended.

[0077] In addition, after sufficiently stabilizing the degree of the vacuum in the absorption chamber **31** (for example, equal to or less than 1×10^{-5} Ps), the elements present on the surface of the multilayer structure body **32** on the absorption chamber **31** side is analyzed by XPS, and thereby the measurement of products is carried out (step S08).

[0078] In addition, the processing in the above-described steps S06 to S07 is repeated, and the change over time of the nuclide transmutation reaction is measured (step S09).

[0079] Additionally, the multilayer structure body **32** is extracted from the nuclide transmutation device **30**, and the experiment on the nuclide transmutation is ended (step S10).

[0080] Below, the results of the two experiments on nuclide transmutation carried out using the nuclide transmutation method according to the present embodiment, that is, the example 1 and example 2 when the identical experiment is carried out two times, will be explained referring to FIG. 7 and FIG. 8.

[0081] FIG. 7 is a graph showing the spectrum of Pr using XPS in the surface of the multilayer structure body **32** shown in FIG. 4, and FIG. 8 is a graph showing the change over time in the number of atoms of Cs and Pr in the surface of the multilayer structure body **32** shown in FIG. 4.

[0082] According to the results of the XPS analysis of the example one and example two, in the example one and the example two the Cs (atomic number $Z=55$) of the multilayer structure body **32** decreases with the passage of time, and for example, like the spectrum of Pr using XPS shown in FIG. 7, the Pr (praseodymium, atomic number $Z=59$) increased.

[0083] Below, the method of calculating the number of atoms of each element from the spectrum of Cs and Pr using XPS will be explained.

[0084] Moreover, the strength of X-rays radiated from the X-ray gun **41** to the multilayer structure body **32** during the measurement by XPS is made constant, and the region in which these X-rays are desorbed is assumed to be identical in each of the measurements of the example one and the example two.

[0085] Furthermore, the region in which the X-rays are emitted on the surface of the multilayer structure body **32** is, for example, a circular region having a diameter of 5 mm, and from the estimation of the escape depth of the photoelectrons that are emitted, the depth that can be analyzed in XPS is, for example, 20×10^{-10} .

[0086] In addition, the Pd that forms the Pd substrate **23** is an fcc (face-centered cubic) lattice, and thus the number of Pd atoms, calculated from the peak strength of the spectrum of Pd obtained by XPS, is 3.0×10^{15} .

[0087] In addition, the number of atoms of each element is calculated by comparing the peak strength of the spectrum of each element obtained by XPS and the peak strength of the spectrum of Pd, referring to the ratio of the ionization cross section of each element, that is, the electrons in the inner shell of the elements, that are excited due to absorbing X-rays and the like. Moreover, in Table 1, the calculated value of the ionization cross section of each element is shown as a relative value in the case that the value of the 1 s orbital of C ($2.22 \times 10^{-24} \text{ m}^2$) is set to '1'. Further, in the following chart 1, 2 p of Si, 2 p of S, and 2 p of Cl are calculated as the sum of $2p_{3/2}$ and $2p_{1/2}$.

TABLE 1

bonding energy of inner shell electrons	ionization		bonding energy of inner shell electrons	ionization	
	cross section			cross section	
C 1s (283.5 eV)	1.00		Mg 2s (88.6 eV)		2.27
O 1s (543.1 eV)	2.29		Pd 3d _{5/2} (335.1 eV)		10.1
Si 2p (99 eV) (*)	0.894		Pd 3d _{3/2} (340.4 eV)		7.03
Si 2s (149.8 eV)	0.884		Cs 3d _{5/2} (726.6 eV)		22.93
S 2p (163 eV) (*)	1.85		Ce 3d _{5/2} (883.9 eV)		28.57
Cl 2p (201 eV) (*)	2.47		Pr 3d _{5/2} (928.8 eV)		30.72

[0088] As shown in FIG. 8, in the first example, under initial conditions, 1.3×10^{14} atoms of Cs were reduced to 8×10^{13} , and after 120 hours, were reduced to 5×10^{13} .

[0089] In contrast, although Pr was not present before the commencement of the experiment, after 48 hours, 3×10^{13} atoms thereof, were detected, and after 12 hours, the number was observed to increase to 7×10^{13} atoms.

[0090] Similarly, in the second example as well, with the passage of time from the commencement of the experiment, a decrease in the number of Cs atoms and Pr production and an increase in the number of Pr atoms was observed, showing a tendency substantially identical to that of the first example. Thus, this can be interpreted as showing that the nuclide transmutation of Cs to Pr was occurring.

[0091] Moreover, in the following, we will consider whether or not the detected Pr is due to contaminants.

[0092] In the first example and the second example of the present embodiment as described above, analysis of elements was carried out without extracting the multilayer structure body 32 from the vacuum container comprising the absorption chamber 31 and the radiation chamber 34, and thus the causes of the introduction of contaminants that can be considered are contaminants included on the deuterium gas (D₂ gas) and contaminants in the multilayer structure body 32.

[0093] In the case of analyzing D₂ gas in the nuclide transmutation device 30 when the D₂ gas is 99.6% pure, and the contaminant N₂ and D₂O are equal to or less than 10 ppm, contaminants O₂, CO₂, and CO are equal to or less than 5 ppm, gases of contaminants other than these contaminants and hydrocarbons were not detected.

[0094] In contrast, in the multilayer structure body 32, the purity of the Pd was 99.5%, and the purities of CaO and CsNO₃ were 99.9%. In addition, as a result of carrying out quantitative analysis of lanthanides (₅₇La to ₇₁Lu) in the multilayer structure body 32 before the commencement of the experiment using glow desorption mass spectrometry (GD-MS), Nd was detected at 0.02 ppm, and the other lanthanides besides Nd were below detection limits, that is, equal to or less than 0.01 ppm.

[0095] Here, if we assume that 0.01 ppm of Pr, which is the detection limit, is present in the multilayer structure body 32 used in the first example and the second example (for example, 0.7 g 7×10^{-3} mol), then the number of Pr atoms present in the multilayer structure body 32 would be 4.2×10^{13} .

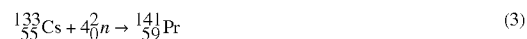
[0096] In this case, based on the above assumption, if we assume that the Pr atoms detected in example 1 and example 2 are Pr atoms below the detection limits, then it is also necessary to assume that all the Pr atoms below the detection limit are disposed so as to be concentrated in the region having a depth of several 10×10^{-10} m from the surface of the multilayer structure body 32, and a physical phenomenon in which the Pr atoms scattered as contaminants in the multilayer structure body 32 are concentrated only in proximity to the surface of the multilayer structure body 32 is thermodynamically impossible. Thus, we cannot conclude that the Pr atoms detected in example one and example two are contaminants included beforehand in the multilayer structure body 32. Furthermore, if they are impurities included beforehand in the multilayer structure body 32, we can determine that there is no time dependent change of the atomic number, that is, a change over time in the number of atoms will maintain a constant value.

[0097] Based on the above, we can conclude that the Pr detected in example one and example two is produced as a result of the nuclide transmutation reaction.

[0098] Moreover, the experimental results of the above-described example one and example two are extremely well explained by the EINR model that appeared in the journal Fusion Technology, published by the US Atomic Energy Conference (Y. Iwamura, T. Itoh, N. Gotoh, and I. Toyoda, "Detection of Anomalous Elements, X-ray, and Excess Heat in a D₂-Pd System and its Interpretation by the Electron-Induced Nuclear Reaction (EINR) Model", Fusion Technology, vol. 33, no. 4, p. 476, 1998).

[0099] According to this EINR model, we can consider the Pr to be produced from Cs according to the Formula (1) and Formula (2).

[0100] Moreover, in the following Formula (1) and Formula (2), d denotes deuterium, e denotes electrons, ₂n denotes dineutrons, and v denotes neutrinos.



[0101] As shown in Formula (2), according to the EINR model, deuterium captures electrons to generate dineutrons, and simultaneously, nuclide transmutation occurs due to reacting with substances such as Cs. Moreover, in Formula (3), the symbols for β^- decay, that is, the β^- decay from ¹⁴¹Cs ($={}^{133}\text{Cs} + 4{}^2_0n$) to ¹⁴¹Pr, have been omitted.

[0102] As described above, according to the nuclide transmutation device 10 of the present embodiment, a relatively large-scale device such as a nuclear reactor or an accelerator are not necessary, and the process of nuclide transmutation can be implemented with a relatively small-scale construction.

[0103] In addition, according to the nuclide transmutation method of the present embodiment, the possibility that the number of atoms of Pr, which are not detected before the

commencement of the experiment and are detected to be increasing after the commencement of the nuclide transmutation experiments, are detected due to contaminants included beforehand in the supplied D₂ gas or in the multilayer structure body **32** is eliminated, and the production of a nuclide transmutation reaction from Cs to Pr can be repeated well and reliably.

[0104] Moreover, in the embodiment described above, the multilayer structure body **32** was formed by adding a cesium (Cs) layer **52** to the surface of the Pd layer **21** as a material that undergoes the nuclide transmutation, but the invention is not limited thereby, and in place of using Cs as a material that undergoes the nuclide transmutation, other materials such as carbon (C) can be added.

[0105] Below, as a first modified example of the present embodiment, the case of adding carbon (C), for example, as a material that undergoes the nuclide transmutation on the surface of the Pd surface **21**, will be explained referring to FIG. **9** and FIG. **10**.

[0106] FIG. **9** is a graph showing the change in the number of atoms for each of C, Mg, Si, and S over time on the surface of the multilayer structure body **32** in the third example, and FIG. **10** is a graph showing the change in the number of atoms for each of C, Mg, Si, and S over time on the surface of the multilayer structure body **32** in the fourth example.

[0107] In this first modified example, the point that differs greatly from the first embodiment described above is the method of forming the multilayer structure body **32**, and in particular, the process in step **S04** described above.

[0108] Specifically, after the step **S03** described above, the multilayer structure body **32** is formed by carbon (C) in the atmosphere adhering to the surface of the Pd layer **21** due to exposing the structure body **11** comprising the Pd substrate **23**, mixed layer **22**, and the Pd layer **21** to the atmosphere (step **S14**).

[0109] In addition, the Pd layer **21** having the adhering C is faced towards the absorption chamber **31**, the absorption chamber **31** and the radiation chamber **34** are closed by interposing the multilayer structure body **32** therebetween, and a vacuum desorption is respectively carried out on both the absorption chamber **31** and the radiation chamber **34**.

[0110] Then the processing in the following the above-described step **S06** is carried out.

[0111] Below, the results of two experiments, that is, the example three and example four when the same experiment according to the first modified example is carried out two times, on nuclide transmutation experiment carried out by the nuclide transmutation method of the modified example of the present embodiment is explained referring to the figures.

[0112] In this case, by the results of the analysis of CPS in example 3 and example 4, in example 3 and example 4, the C in the multilayer structure body **32** decreases with the passage of time, and Si and S, which are reaction products, and Mg, which is an intermediate product, were detected.

[0113] In addition, similar to the embodiment described above, the number of atoms of each element is calculated from the spectrum of C, Mg, Si, and S by XPS.

[0114] As shown in FIG. **9**, in example 3, the number of C atoms originating in hydrocarbons decreased 44 hours after the commencement of the experiment, while Mg, which was not present before the commencement of the experiment, was detected 44 hours later, and furthermore, had somewhat decreased after 116 hours.

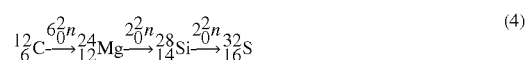
[0115] Furthermore, Si and S, which were not present before commencement of the experiment, increased monotonically 44 hours later and 116 hours later.

[0116] As shown in FIG. **10**, in example 4, the number of C atoms originating in hydrocarbons decreased monotonically 24 hours, 76 hours, and 116 hours after the commencement of the experiment, while in contrast Mg, which was not present before the commencement of the experiment, was produced 24 hours after commencement, and furthermore, monotonically decreased after 76 and 116 hours.

[0117] Furthermore, Si and S, which were not present before commencement of the experiment, monotonically increased 24, 76, and 116 hours after commencement.

[0118] According to the above results, the nuclide transmutation method according to the modified example of the present invention resulted in C being transmuted, and Mg, Si, and S being generated.

[0119] In this case, according to the EINR model described above, the nuclide transmutation of C is represented in Formula (2) described above and Formula (4). Moreover, in Formula 4, a reaction by a dineutron cluster (6^2n , 2^2n) is represented.



[0120] Below, the second modified example of the present embodiment is explained with reference to FIGS. **11** to **17** when, for example, strontium (Sr) is added on the surface of the Pd layer **21** as an element that undergoes nuclide transmutation.

[0121] FIG. **11** is a cross-sectional structure diagram showing the multilayer structure body **32** related to the second modified example of the present embodiment. FIG. **12** is a graph showing the XPS spectrum of the Mo element on the surface of the multilayer structure body **32** shown in FIG. **11**. FIGS. **13** and **14** show a time dependent change of atomic numbers of respective Sr and Mo elements on the surface of the multilayer structure body **32**. FIG. **15** shows the change of a isotopic ratio and the atomic mass number of natural Mo. FIG. **16** shows the change of an isotopic ratio and the atomic number of Mo observed on the multilayer structure body **32** in the fifth embodiment. FIG. **17** is a graph showing the change of the isotopic ratio and the atomic mass number of the natural Sr added as a material that undergoes nuclide transmutation.

[0122] In this second modified example, the Sr layer **53** is added on the multilayer structure body **32** in place of the Cs layer **52** used for being subjected to the nuclide transmutation. That is, the point of the second modified example which differs from the above-described first modified example is the method of forming the multilayer structure body **32**, particularly, the processing in step **S04**. Note that, in the second modified example, the platinum substrate **23** has a size of 25 mm×25 mm×0.1 mm (length×width×thickness) and having a impurity of more than 99.9%.

[0123] In the second modified example, after the above-described step **S03**, Sr, for example, is added as the material that undergoes nuclide transmutation on the film formed surface of the structure body by electrolysis of a diluted solution of SrO in D₂O (Sr(OD)₂/D₂O solution) on the film forming surface of the multilayer structure body **11**. In the electrodeposition device **60**, for example, shown in FIG. **6**, 1 mM

of the $\text{Sr}(\text{OD})_2/\text{D}_2\text{O}$ solution is used, and electrolysis is carried out, for example, for 10 seconds at 1V after connecting the anode of the power source **61** to the platinum anode **63** and connecting the cathode of the power source **61** to the multilayer structure body **11**. The chemical reaction shown by the formula (5) takes place by the electrolysis, and the Sr layer **53** is deposited on the surface of the multilayer structure body **32** (step **S04a**)



[0124] Subsequently, the Sr layer **53** of the multilayer structure body **53** is directed to the absorption chamber **31** and the processes below step **S05** are conducted.

[0125] Hereinafter, two results of the nuclide transmutation experiments, that is, the results of the example 5 and example 6, which were conducted by repeating the same experiment for two times in line with the nuclide transmutation method according to the second modified example of the present embodiment are described.

[0126] The analysis of XPS obtained in the example 5 and example 6 indicated that Sr (the atomic number $Z=38$) on the multilayer structure body **32** has been decreased with the passage of time, and Mo (molybdenum, $Z=42$) has been increased as shown by the Mo spectrum of XPS in FIG. **12**.

[0127] The calculation of the number of atoms of Sr and Mo from the XPS spectrum of Sr and Mo are conducted by the same method as that in the first embodiment.

[0128] That is, it is assumed that the intensity of the X-ray irradiated on the multilayer structure body **32** from the X-ray gun during XPs measurement is constant and that the regions irradiated by X-ray for the measurements in example 5 and example 6 are the same.

[0129] Furthermore, it is also assumed that the region on the multilayer structure body **32** irradiated by X-rays is, for example, a circle with a diameter of 5 mm and that the measurable surface thickness by XPS is 20×10^{-10} m from the estimation of the depth of the photoelectrons escaped from the surface.

[0130] The number of atoms of Pd is assumed to be 3×10^{15} based on the peak intensity of the Pd spectrum obtained by XPS, assuming that the Pd constituting the Pd substrate is composed of a face centered cubic (fcc) crystal.

[0131] The number of atoms of each elements is calculated by comparison of the peak intensity of each element with the peak intensity of the Pd spectrum obtained by XPS, with reference to the ionization cross section of each element, that is, the ratio of inner-shell electrons excited by absorbing X-rays.

[0132] As shown in FIG. **13**, it has been observed that, in example 5, the number of atoms of 1.2×10^{14} of Sr present at the initial condition is reduced to 1.0×10^{14} after 80 hours, and further reduced to 8×10^{13} after 400 hours.

[0133] In contrast, it was observed that 2.2×10^{13} atoms of Mo, which were not present before starting the experiment, were observed after 80 hours, and the number of atoms of Mo was increased to 3.2×10^{13} after 240 hours, and was further increased to 3.8×10^{13} after 400 hours.

[0134] Similarly, in experiment 6 shown in FIG. **14**, the same tendency as the case of example 5 was observed. That is, the number of Sr atoms is reduced with the passage of time, and generation and an increase of number of Mo atoms, which is not present at the initial condition, are observed.

[0135] Furthermore, in both examples 5 and 6, since the time dependent reduction number of Sr atoms approximately

conforms with the time dependent increasing number of Mo atoms, this tendency is interpreted to mean that the nuclide transmutation occurs from Sr to Mo. Consequently, it is possible to mention that the experiments in both examples 5 and 6 yield reproducible results.

[0136] In addition, in example 5, the isotopic ratio of Mo generated by the experiment is calculated through an analysis of the surface of the multilayer structure body **32** using SIMS (Secondary Ion Mass Spectroscopy) after the above-described step **S10**.

[0137] As shown in FIG. **6**, the isotopic ratio of Mo observed in example 5 when compared to that of the isotopic ratio of the natural Mo indicates that a particular isotope of Mo, that is, ^{96}Mo , shows a dramatically high abundance ratio.

[0138] As shown in FIG. **17**, the isotopic ratio of the natural Sr added to the multilayer structure body **32** indicated that a particular isotope of Sr, that is, ^{88}Sr , shows a remarkably high abundance ratio. The above results clearly indicate that there is a strong correlation between the isotopic ratio of a nuclide (Sr) that undergoes nuclide transmutation and the isotopic ratio of the material (Mo) observed after the experiment, so that it can be concluded that the Mo detected in examples 5 and 6 is generated by the nuclide transmutation of Sr.

[0139] Furthermore, the experimental results of examples 5 and 6 are quite well explainable by the above-mentioned EINR model, and it is possible to explain that ^{96}Mo is formed by the reaction shown in equations (2) and (6), which is described later.

[0140] Note that the letter symbol of β^{-} decay, that is, the decay of ^{96}Sr ($=^{88}\text{Sr} + 4^2\text{n}$) towards ^{96}Mo , is omitted.



[0141] Below, the nuclide transmutation device and nuclide transmutation method according to the second embodiment of the present invention will be explained referring to the figures.

[0142] FIG. **18** is a drawing for explaining the principle of the nuclide transmutation method according to the second embodiment of the present invention. FIG. **19** is a structural diagram of the nuclide transmutation device according to the second embodiment of the present invention.

[0143] As shown, for example, in FIG. **18**, the device **70** for realizing the nuclide transmutation method according to the present embodiment comprises an anode **71** of platinum and the like, a cathode **72** comprising palladium (Pd) or a Pd alloy, or another metal that can absorb hydrogen (for example, Ti and the like), or an alloy thereof, a heavy water solution **73** into which the cathode **71** and one surface of the cathode **72** are immersed, an electrolyte cell **74** made fluid-tight by the cathode **72** and filled with the heavy water solution that includes material that undergoes the nuclide transmutation, and a vacuum container **75** sealed air-tight by the anode **72**, and wherein a flow of deuterium is generated in the cathode **72** by one surface **72A** side of the cathode **72** being made a region having a high deuterium pressure due to electrolysis and the like, and the other surface **72B** side being made a region having a low deuterium pressure due to vacuum evacuation and the like, and the nuclide transmutation is carried out by a reaction between the deuterium and the material that undergoes nuclide transmutation.

[0144] Here, the cathode 72 has a structure identical, for example, to the structure body 11 shown in FIG. 2, and preferably, a mixed layer 22 of a material having a relatively low work function, that is, a material that emits electrons easily (for example, a substance having a work function less than 3 eV), and Pd is formed on the surface of the Pd substrate 23, and the Pd layer 21 is formed by lamination on the surface of this mixed layer 22.

[0145] As shown in FIG. 19, the nuclide transmutation device 80 according to the present embodiment comprises a power source 81, an electrolytic cell 83 providing a voltmeter 82, an electrolytic solution 84 stored in the electrolyte cell 83, a vacuum container 85, a spiral refrigerating tube 86 made, for example, of an insulating resin that freezes the electrolytic solution 84 in the electrolyte cell 86, a catalyst 87, an anode electrode 88 of platinum and the like that is connected to the anode of the power source 81 and is immersed in the electrolytic solution 84, a multilayer structure body 89 that maintains the electrolyte cell 83 in a liquid-tight condition and at the same time maintains the vacuum container 85 in an airtight state and is connected to the cathode of the power source 81, a thermostat 90 that accommodates the electrolyte cell 83 and the vacuum container 85 and controls the temperature, and a vacuum exhaust pump 91 that places the vacuum container 85 in a vacuum state.

[0146] Here, the electrolyte cell 83 made, for example, of an insulating resin and the vacuum container 85 made, for example, of stainless steel, are sealed in liquid-tight and airtight states by the multilayer structure body 89 via, for example, a Culret's O-ring, and so to speak, connected via the multilayer structure body 89.

[0147] In addition, the electrolyte solution 84 stored in the electrolyte cell 83 is a heavy water solution that includes, for example, cesium (Cs) as a material that undergoes nuclide transmutation. This electrolyte solution 84 may be a Cs₂(SO₄) heavy water solution having a concentration, for example, of 3.1 mol/L.

[0148] Moreover, the catalyst 87 is formed by electrodepositing platinum black on platinum, water is produced from most of the hydrogen and oxygen generated by the electrolysis of the electrolytic solution 84, and this is returned to the electrolyte solution 84.

[0149] The nuclide transmutation device according to the present embodiment provides the structure described above, and next the method of carrying out nuclide transmutation using this nuclide transmutation device 80 will be explained referring to the figures.

[0150] First, the structure body 11 is produced in a manner identical to the step S01 to step S03 in the nuclide transmutation method in the above-described first embodiment.

[0151] In addition, this structure body 11 serves as the multilayer structure body 89, the Pd layer 12 of the multilayer structure body 89 is faced towards the electrolytic cell 83 side, and the electrolytic cell 83 and the vacuum container 85 are sealed in respectively liquid-tight and air-tight states (step S21).

[0152] Next, a Cs₂(SO₄) heavy water solution having a concentration, for example, of 3.1 mol/L is injected as an electrolytic solution 84 in the electrolytic cell 83. Furthermore, the space in the electrolytic cell 83 not filled by the electrolytic solution 84 is filled with nitrogen gas and sealed, and the pressure in the electrolytic cell 83 is maintained at, for example, 1.5 kg/cm² (step S22).

[0153] In addition, the vacuum container 85 is evacuated by a vacuum pump 91, and maintained in a vacuum state (step S23).

[0154] Additionally, a refrigerant is supplied to a refrigerant pipe 86 made of an insulating resin and the like, and the temperature in the electrolytic cell 83 is maintained at a predetermined constant temperature (step S24).

[0155] In addition, an anode electrode 88 made, for example, of platinum, and the multilayer structure body 89 serving as the cathode, which are immersed in the electrolytic solution 84 in the electrolytic cell 83, are connected to the power source 81, and the electrolytic reaction is generated by the power supplied from the power source 81 (step S 25).

[0156] Here, the current supplied during the electrolysis is gradually raised from 1 A to 2 A over a three hour interval, and subsequently maintained at 2 A.

[0157] In addition, after commencement of the electrolysis, the temperature of the thermostat 90 is set to 70° C. after 12 hours, and the temperature is thereafter maintained at this temperature (step S26).

[0158] This electrolysis is suspended after a predetermined time interval, for example, 7 days, and the temperature of the thermostat 90 is set to room temperature (step S27).

[0159] In addition, the multilayer structure body 89 is extracted from the nuclide transmutation device 80, and the surface of the multilayer structure body 89 is analyzed by secondary ion mass spectroscopy (SIMS) (step S28).

[0160] Below, the results of experiments using the nuclide transmutation experiment carried out using the nuclide transmutation method according to the present embodiment described above, that is, example seven, are explained referring to FIG. 20 and FIG. 21.

[0161] FIG. 20 is a drawing showing the surface on the electrolyte cell side of the multilayer structure body after experiments using the nuclide transmutation device shown in FIG. 19, and FIG. 21 is a graph showing the results of the SIMS analysis of the surface of the multilayer structure body after experiments using the nuclide transmutation device shown in FIG. 19.

[0162] With respect to the part 96 shown in FIG. 20 that the deuterium penetrates and the part 95 shown in FIG. 20 that the deuterium does not penetrate, as shown in FIG. 21, for ¹⁴⁰Ce the intensity of secondary ions agree, but for ¹³⁹La and ¹⁴¹Pr, the part not penetrated by the deuterium, that is, the part in which the nuclide transmutation reaction was produced, the intensity of the secondary ions became large.

[0163] In addition, although it is not possible to distinguish whether the mass number A 142 is ¹⁴²Ce or ¹⁴²Nd, the intensity of the secondary ions became large in the part 96 that the deuterium penetrated.

[0164] Thereby, it can be concluded that at least ¹⁴¹Pr is a substance formed by the nuclide transmutation of Cs.

[0165] As described above, according to the nuclide transmutation device 80 of the present embodiment, a relatively large-scale device such as a nuclear reactor or accelerator are unnecessary, and the nuclide transmutation process can be carried out with a relatively small-scale structure.

[0166] Furthermore, while the structure differs from the nuclide transmutation device 30 according to the first embodiment described above, experimental results were obtained showing that the nuclide transformation reaction from Cs to Pr is produced, and the effectiveness of the essential means of the present invention can be shown.

[0167] In addition, according to the nuclide transmutation method of the present embodiment, in the multilayer structure body **89**, from a comparison of the part **96** that the deuterium penetrated and the part **95** that the deuterium did not penetrate, it can be reliably shown that at least a nuclide transmutation reaction from Cs to Pr is produced.

[0168] Moreover, in the present embodiment, a heavy water solution that includes a material that undergoes the nuclide transmutation was used as the electrolyte solution **84**, but the invention is not limited thereby, and on one surface of the multilayer structure body **89**, a substance that undergoes nuclide transmutation, for example Cs can be laminated by a film formation process such as vacuum deposition or sputtering, and the surface on which this Cs is laminated is faced towards the electrolytic cell **83**, and immersed in an electrolytic solution **84** comprising the heavy water solution stored in the electrolytic cell **83**. In this case, including a substance, for example, Cs, that undergoes nuclide transmutation in the heavy water solution is not necessary.

[0169] Moreover, in the present embodiment described above, the heavy water solution that includes Cs as the electrolyte solution **84** is used, but the invention is not limited thereby, and instead of Cs, another material such as sodium (Na) can be added as the material that undergoes the nuclide transformation.

[0170] Below, as a modified example of the present embodiment, the case in which sodium (Na) is added to the heavy water solution as the material that undergoes the nuclide transmutation will be explained.

[0171] In this modified example, the major point of difference with the second embodiment described above is the processing from step S22 and subsequent steps, as described above.

[0172] Specifically, after the above-described step S21, only, for example, 400 ppm of sodium is added as the electrolyte solution **84** in the electrolyte cell **83**, and LiOD heavy water solution having a concentration of 4.3 mol/L is injected.

[0173] Furthermore, the contents of the space not filled by the electrolyte solution **84** in the electrolyte cell **83** is filled with nitrogen gas and sealed, and the pressure in the electrolyte cell **83** is maintained at, for example, 1.5 kg/cm² (step S32).

[0174] In addition, the inside of the vacuum container **85** is evacuated by the vacuum pump **91**, and is maintained in a vacuum state (step S33).

[0175] Additionally, a refrigerant is supplied into the refrigeration tube **86** made, for example, from an insulating resin, and the temperature in the electrolyte cell **83** is maintained at a predetermined constant temperature (step S34).

[0176] In addition, the anode electrode **88** that is made from platinum and the like and immersed in the electrolyte solution **84** in the electrolyte cell **83** and the multilayer structure body **89** serving as a cathode are connected to the power source **81**, and an electrolytic reaction is produced due to the power supplied from the power source **81** (step S35).

[0177] Here, the current supplied during electrolysis is gradually raised over, for example, a six hour interval from 0.5 A to 2 A, and subsequently maintained at 2 A.

[0178] In addition, this electrolysis is suspended after a predetermined interval, for example, after continuing for 7 days, and the temperature of the thermostat **90** is set to room temperature (step S36).

[0179] Additionally, the multilayer structure body **89** is extracted from the nuclide transmutation device **80**, and the

surface of the multilayer structure body **89** is analyzed using electron probe microanalysis (EPMA) (step S 37).

[0180] Below, the experimental results of three nuclide transmutation experiments carried out using the nuclide transmutation method according to the modified examples of the second embodiment of the present invention described above, that is, example 8, example 9, and example 10, which are the same experiment carried out three times.

[0181] Moreover, in the following Table 2, for example 8, example 9, and example 10, the results of the analysis of the electrolyte solution **84** using inductive coupled plasma-Auger electron spectrometry (ICP-AES) are shown. Moreover, the results of analysis of the electrolyte solution **84** before the commencement of the experiments are shown as comparative examples.

TABLE 2

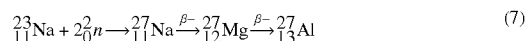
	Comparison example	Example six	Example seven	Example eight	
Na	430	25	16	56	(ppm)
	0.086	0.005	0.003	0.011	(g)
	2.3×10^{21}	1.3×10^{20}	8.4×10^{19}	2.9×10^{20}	(Atoms)
Al	<1	410	420	310	(ppm)
	$<2 \times 10^{-4}$	0.082	0.084	0.062	(g)
	$<2 \times 10^{18}$	1.8×10^{21}	1.9×10^{21}	1.4×10^{21}	(Atoms)

[0182] As shown in Table 2, in the electrolyte solution **84** before the commencement of the experiments, the Na was at 430 ppm, and Al was equal to or less than the detection limit of 1 ppm.

[0183] In contrast, after the nuclide transmutation experiment, the Na became several tens of ppm, a value being one order lower, and the Al had become several tens of a ppm. The change in the electrolyte solution **84** after the commencement of the experiment carried out only electrolysis by providing current from the power source **81**, and other materials were not introduced from the outside.

[0184] In addition, regarding the number of atoms (Atom, in Table 2), it could be confirmed that the decreased number of Na atoms fell from 2.2×10^{21} to about 2.0×10^{21} , and the increased amount of the Al substantially agreed with this.

[0185] This result is represented by the above Formula (2) and the following Formula (7) in the EINR model described above.



[0186] Here, for Na, the natural abundance of ²³Na is 100%, and for Al, the natural abundance of ²⁷Al is 100%. It can be inductively determined from past experimental data that nuclide transmutation is easily produced between nuclides having similar isotopic ratio compositions, and it can be inferred that the possibility that Na transmutes to Al is high since the isotopes that exists stably for both elements Na and Al are unique.

[0187] In addition, as a result of analysis of the multilayer structure body **89** using EPMA, Al was detected from the central part of the multilayer structure body **89**, that is the part that the deuterium penetrated. Because Al is an amphoteric metal, it can be electrolyzed in the electrolytic solution **84**, but by detecting Al from the center part of the surface of the

multilayer structure body **89**, we can conclude that Al was produced by the nuclide transmutation of Na.

[0188] Moreover, in the present embodiment, a heavy water electrolyte solution that includes a material that undergoes the nuclide transmutation is used, but the invention is not limited thereby, and on one of the surfaces of the multilayer structure body **89**, a material that undergoes nuclide transmutation, for example, Na, can be laminated using a film formation method such as vacuum deposition or sputtering, the surface on which this Na has been laminated can be faced towards the inside of the electrolytic cell **83**, and this can be immersed in the electrolytic solution **84** comprising the heavy water solution stored in the electrolyte cell **83**. In this case, it is not necessary to include a material that undergoes the nuclide transmutation in the heavy water solution, that is, Na.

[0189] Below, the nuclide transmutation device and the nuclide transmutation method according to the third embodiment of the present invention are explained with reference to the attached drawings.

[0190] FIG. 22 shows a structure of the nuclide transmutation device **100** according to the third embodiment of the present invention.

[0191] The nuclide transmutation device **100** according to this embodiment comprises a desorption chamber **101** having an interior that can be maintained in an airtight state, an absorption chamber **103**, disposed inside of the desorption chamber **101** and having an interior that can be maintained in an airtight state through a multilayer structure body **102**, a deuterium tank **106** for supplying deuterium into the absorption chamber **103** through a regulator valve **104** and a valve **105**, a pressure meter **107** for detecting the inside pressure of the absorption chamber **103**, a connecting pipe **109** for connecting the desorption chamber **101** and an absorption chamber **103** through a vacuum valve **108**, a turbo-molecular pump **110** for maintaining the inside of the desorption chamber **101**, a rotary pump for preliminary evacuation of the desorption chamber **101**, the absorption chamber **103**, and the turbo-molecular pump **110**, and a vacuum gauge **112** for detecting the degree of vacuum in the desorption chamber **101**.

[0192] The nuclide transmutation method using the above-described nuclide transmutation device **100** according to this embodiment will be described below with reference to the attached drawings.

[0193] First, a platinum substrate **23** (for example, having a size of 70 mm in diameter and 0.1 mm in thickness and a purity of more than 99.9%) shown in, for example, FIG. 2, is degreased by ultrasonic cleaning in acetone over a predetermined time. Then, the substrate is heat treated, that is, annealed at a temperature of, for example, 900° C., in an argon atmosphere (step S42).

[0194] Subsequently, the platinum substrate **32**, after the annealing process, is subjected to etching, for example, using a 1.5 times diluted aqua regia at room temperature for a predetermined time (for example, 100 seconds) to remove impurities on the substrate surface (step S42).

[0195] Next, similarly to the above-described step S03, a multilayer structure body is formed by depositing films on the platinum substrate **23** after the etching process by a sputtering method using an argon beam.

[0196] Furthermore, a multilayer structure body **102** is formed by addition of a Cs layer that undergoes nuclide transmutation on the film deposited surface of the multilayer structure body **11** by electrolysis of the D₂O diluted solution of CsNO₃ (CsNO₃/D₂O solution) (step S44).

[0197] The desorption chamber **103** and the absorption chamber **101** is closed so as to be airtight after the Cs layer of the multilayer structure body **102** is directed towards the absorption chamber **103**. Then, the valve **105** is closed, the vacuum valve **108** in the connecting pipe **109** is opened, and the desorption chamber **101** and the absorption chamber **103** are evacuated using the rotary pump **111** and the turbo-molecular pump **110** (step S45).

[0198] Subsequently, after the multilayer structure body **102** is heated to, for example, 70° C. by a heating device (not shown), the vacuum valve **108** is closed and evacuation of the absorption chamber **103** is stopped. Then, deuterium gas is introduced into the absorption chamber **103** at a predetermined pressure and the experiment of the nuclide transmutation is commenced. The predetermined pressure at the time of introducing the deuterium gas is regulated by the regulator valve **104**, and the pressure is determined, for example, to be 1.01325×10⁵ (1 atm) (step S46).

[0199] The amount of the deuterium gas discharged in the desorption chamber **101** is calculated based on the degree of vacuum detected by, for example, the vacuum gauge **112** and the flow rate of the turbo-molecular pump **110**.

[0200] After several tens of hours after starting introduction of the deuterium gas in the absorption chamber **103**, the temperature of the multilayer structure body **102** is returned to room temperature. The valve **105** is closed and after stopping the introduction of the deuterium gas into the absorption chamber **103**, the absorption chamber **103** is evacuated and the nuclide transmutation experiment is completed (step S47).

[0201] The multilayer structure body **102** is taken out from the nuclide transmutation chamber **100** and the multilayer structure body **102** is etched by aqua regia for preparing a solution which contains the elements present on the surface of the multilayer structure body **102**. This solution is analyzed by an ICP-MS (Inductive Coupled Plasma-Mass spectrometry) for quantitative analysis of the elements present on the surface of the multilayer structure body **102** (step S48).

[0202] Below, the results of two repeated experiments by the same method, that is, the experiments 11 and 12, based on the same nuclide transmutation method according to the above-described embodiment of the present invention are described.

[0203] In the following Table 3, the results of the ICP-MS analyses for two samples obtained in the examples 11 and 12 are described.

TABLE 3

	Pr	Cs
Example 11	1.3 μg	2.3 μg
Comparative Example	0.008 μg	3.8 μg
Example 12	0.12 μg	—

[0204] As shown in Table 3, it was found that the contents of Pr and Cs were 0.008 μg and 3.8 μg, respectively, in the solution of the comparative example, which is obtained from the multilayer structure body **102** before starting the experiments

[0205] In contrast, after the experiments of the nuclide transmutation, the content of Pr is increased to 1.3 μg, which is more than 100 times greater than the initial weight, and the content of Cs is decreased to 2.3 μg.

[0206] In the experiment 12, the content of Pr increases to 0.12 μg , which corresponds to a weight more than ten times greater than the initial weight.

[0207] Consequently, it is concluded that the above results indicate that the increase of Pr observed in examples 11 and 12 is caused by the nuclide transmutation from Cs to Pr.

[0208] As described above, although the nuclide transmutation device 100 according to the present invention has a relatively small-scale structure, it is confirmed that the present nuclide transmutation device is able to carry out nuclide transmutation instead of using large scale systems such as a nuclear reactor or a particle accelerator.

[0209] In addition, in spite of the fact that the present nuclide transmutation device and the multilayer structure body differ from the nuclide transmutation device 30 and the multilayer structure body according to the first embodiment, both of the nuclide transmutation devices and multilayer structure bodies are confirmed to be able to carry out the nuclide transmutation such as from Cs to Pr successfully, which results in showing the substantial effectiveness of the present invention.

[0210] In addition, in the first embodiment, the second embodiment, and the third embodiment of the present invention described above, palladium (Pd) was used as the metal for absorbing the hydrogen, but the invention is not limited thereby, and a Pd alloy, or, for example, another metal that absorbs hydrogen, such as Ti, Ni, V, or Cu, or an alloy thereof can be used.

[0211] As explained above, according to the first aspect of the nuclide transmutation device of the present invention, nuclide transmutation can be carried out with a relatively small-scale device compared to the large-scale devices such as accelerators and nuclear reactors, a pressure differential in the deuterium between the one surface and the other surface of the structure body is provided, and within the structure body a flux of deuterium from one surface side to the other surface side is produced, and thereby an easily reproducible nuclide transmutation reaction can be produced for the deuterium and the material that undergoes nuclide transmutation.

[0212] Furthermore, according to the second aspect of the nuclide transmutation device of the present invention, the absorption part is pressurized by the deuterium supply device, and at the same time, the pressure in the radiation part is reduced to a vacuum state by the exhaust means, and thus a pressure differential in the deuterium is formed in the structure body.

[0213] Furthermore, according to the third aspect of the nuclide transmutation device of the present invention, by electrolyzing the electrolytic solution on one surface of the structure body with the structure body serving as a cathode, deuterium is absorbed effectively into the structure body due to the high pressure, and by reducing the pressure of the radiation part to a vacuum state using the exhaust device, a pressure differential in the deuterium is formed in the structure body.

[0214] Furthermore, according to the fourth aspect of the nuclide transmutation device of the present invention, the transmutation material lamination device can laminate the material that undergoes the nuclear transmutation on one surface of the structure body by a surface forming process, such as electrodeposition, vapor deposition, or sputtering.

[0215] Furthermore, according to the fifth aspect of the nuclide transmutation device of the present invention, the material that undergoes nuclide transmutation can be bound

to one surface of the structure body by mixing the material that undergoes nuclide transmutation in, for example, a gas or liquid that includes deuterium.

[0216] Furthermore, according to the sixth aspect of the nuclide transmutation device of the present invention, a mixed layer that includes a material having a low work function is provided on the structure body that serves as the multilayer structure, and thereby the repeatability of the production of the nuclide transmutation reaction is improved.

[0217] Moreover, according to the first through sixth aspects of the nuclide transmutation device of the present invention, the production of the nuclide transmutation reaction can be further promoted by transmuting the material that undergoes nuclide transmutation to a nuclide having a similar isotope ratio composition, and the repeatability of the generation of the nuclide transmutation reaction can be improved.

[0218] In addition, according to the seventh aspect of the nuclide transmutation device of the present invention, a flux of deuterium from the one surface side to the other surface side within the structure body is produced, and thereby the nuclide transmutation reaction is produced with good repeatability for the deuterium and the material that undergoes nuclide transmutation.

[0219] Furthermore, according to the eighth aspect of the nuclide transmutation method of the present invention, a material that undergoes nuclide transmutation is laminated on the one surface of the structure body by a film formation process using a transmutation material lamination process such as electrodeposition, vaporization deposition, or sputtering, or the material that undergoes nuclide transmutation is mixed with a gas or liquid that includes deuterium and the like, and thereby the material that undergoes the nuclide reaction is bound to the one surface of the structure body.

[0220] Furthermore, according to the ninth aspect of the nuclide transmutation method of the present invention, the material that undergoes nuclide transmutation is transmuted to a nuclide having a similar isotopic ratio composition, and thereby the nuclide transmutation reaction can be promoted, and the repeatability of the generation of the nuclide transmutation reaction can be improved

1. A nuclide transmutation device comprising:

- a structure body including a hydrogen absorbing material which is at least one of a hydrogen absorbing metal and a hydrogen absorbing alloy, and which comprises a low work function material having a work function equal to or less than 3 eV;
- an absorption part in which one surface of said structure body is exposed to a deuterium gas at a pressure;
- a desorption part in which another surface of said structure body is exposed to the deuterium gas at a pressure lower than the pressure in said absorption part, said desorption part and said absorption part being positioned to form a closed space sealed by said structure body;
- a high pressurization device configured to produce the pressure in said absorption part, said high pressurization device including a deuterium supply device configured to supply the deuterium gas to said absorbing part;
- a low pressurization device configured to reduce the pressure in said desorption part, said low pressurization device including an exhaust gas device configured to evacuate said desorption part;

a transmutation material binding device configured to bind a material that undergoes nuclide transmutation on said one surface of said structure body; and
 a heating device that controls the temperature of the structure body,
 wherein the high pressurization device and the low pressurization device are configured to provide a flow of the deuterium that penetrates through the structure body and the material bound on the structure body.

2. A nuclide transmutation device according to claim 1, wherein said transmutation material binding device comprises a transmutation material lamination device configured to laminate said material that undergoes nuclide transmutation on said one surface of said structure body.

3. A nuclide transmutation device according to claim 1, wherein said transmutation material binding device includes a transmutation material supply device configured to supply said material that undergoes nuclide transmutation to said absorption part, and expose said one surface of said structure body to a gas or liquid that includes said material that undergoes the nuclide transmutation.

4. A nuclide transmutation device according to claim 1, wherein said structure body includes:
 a base material including a hydrogen absorbing metal or a hydrogen absorbing alloy;
 a mixed layer formed on said base material and comprised of at least one of the hydrogen absorbing metal and the hydrogen absorbing alloy, and a material comprised of the low work function equal to or less than 3 eV; and
 a surface layer formed on said mixed layer and comprised of at least one of the hydrogen absorbing metal and the hydrogen absorbing alloy.

5. A nuclide transmutation device according to claim 1, wherein the transmutation material includes at least one of Cs, C, Sr, and Na.

6. A nuclide transmutation device according to claim 1, wherein the structure body comprises a substrate including Pd, a mixed layer formed on the substrate and including Pd and a material having a work function equal to or less than 3 eV, and a layer formed on the mixed layer and including Pd.

7. A nuclide transmutation device according to claim 6, wherein the mixed layer comprises layers including CaO and layers including Pd that are laminated alternately.

8. A nuclide transmutation device according to claim 1, wherein the absorption part comprises an absorption chamber, the desorption part comprises a radiation chamber, the high pressurization device comprises a deuterium tank configured to supply the deuterium gas into the absorption chamber, and the low pressurization device comprises a vacuum pump configured to maintain an interior of the radiation chamber in a vacuum state.

9. A nuclide transmutation device according to claim 1, wherein said structure body comprises palladium or a palladium alloy.

10. A nuclide transmutation device comprising:

a structure body which includes a hydrogen absorbing material which is at least one of a hydrogen absorbing metal and a hydrogen absorbing alloy, and which comprises a low work function material having a work function equal to or less than 3 eV, the structure body having one surface on which a material that undergoes nuclide transmutation is provided;

an absorption part in which said one surface of said structure body is exposed to a deuterium gas at a pressure;

a desorption part in which another surface of said structure body is exposed to the deuterium gas at a pressure lower than the pressure in said absorption part, said desorption part and said absorption part being positioned to form a closed space sealed by said structure body;

a high pressurization device configured to produce the pressure in said absorption part, said high pressurization device including a deuterium supply device configured to supply the deuterium gas to said absorbing part;

a low pressurization device configured to reduce the pressure in said desorption part, said low pressurization device including an exhaust gas device configured to evacuate said desorption part, and

a heating device that controls the temperature of the structure body,

wherein the high pressurization device and the low pressurization device are configured to provide a flow of the deuterium that penetrates through the structure body and the material provided on the structure body.

* * * * *