

[54] **IMPROVED PROCESS FOR PRODUCING UNIFORMLY PLATED MICROSPHERES**

[76] **Inventor:** James A. Patterson, 2074 20th St., Sarasota, Fla. 34234

[21] **Appl. No.:** 353,260

[22] **Filed:** May 16, 1989

[51] **Int. Cl.⁵** C25D 7/00; C23C 18/18

[52] **U.S. Cl.** 204/20; 204/30; 427/222; 427/306; 427/443.1

[58] **Field of Search** 427/214, 215, 216, 217, 427/222, 306, 443.1; 204/20, 30

[56] **References Cited**

U.S. PATENT DOCUMENTS

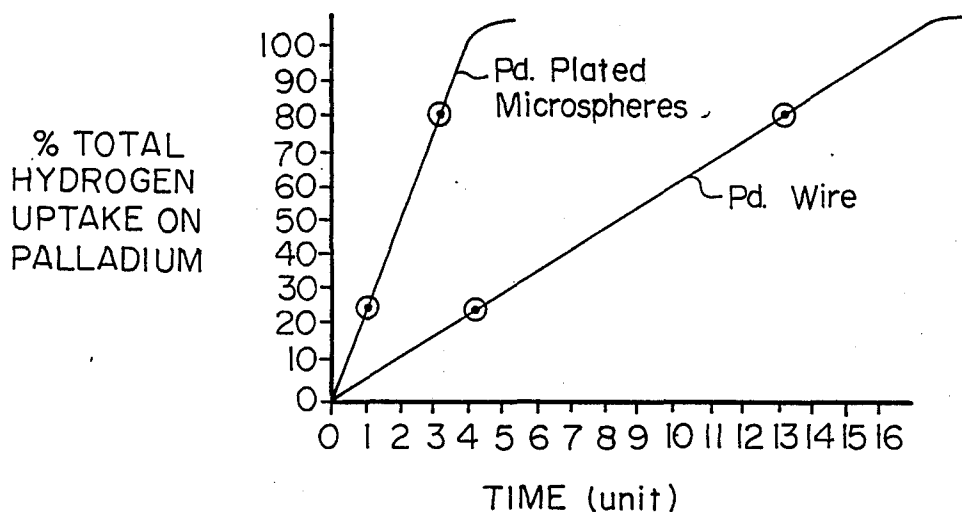
2,915,406	12/1959	Rhoda et al.	428/655 X
3,577,324	5/1971	Patterson	204/20
3,654,098	4/1972	Backhurst et al.	204/20
3,991,225	11/1976	Blouin	427/3
4,243,728	1/1981	Sato et al.	428/570
4,316,786	2/1982	Yu et al.	204/223
4,564,532	1/1986	Henderson	427/2
4,624,865	11/1986	Gindrup et al.	427/126.2

Primary Examiner—John F. Niebling
Assistant Examiner—William T. Leader
Attorney, Agent, or Firm—Charles J. Prescott; Raymond H. Quist

[57] **ABSTRACT**

Cross-linked polymer microspheres are carefully separated into fractions of equal size and density by first using sieves and then using hydraulic separation in a cone. Each fraction is separately plated with copper. The copper plated microspheres are again separated into fractions of equal size and density. Each fraction is then given an additional metal plating. The thus plated microspheres have uniformly thick plating and have a maximized surface area for the amount of metal plated making them particularly useful as catalysts or in electrical products or processes. Microspheres having a plating of palladium exhibit a marked improvement in the adsorption of hydrogen both quantitatively and in rapidity.

16 Claims, 1 Drawing Sheet



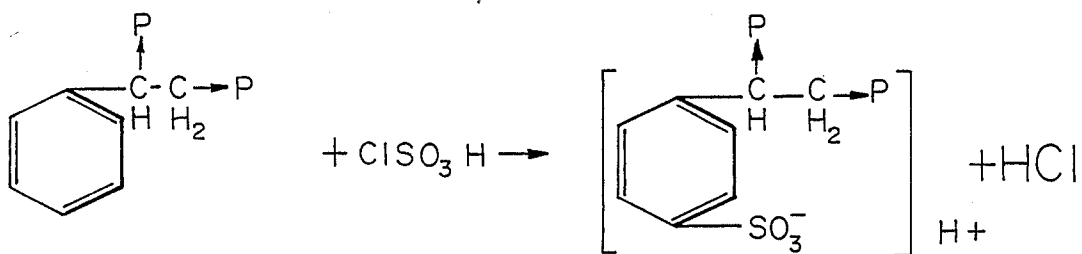


FIG. 1

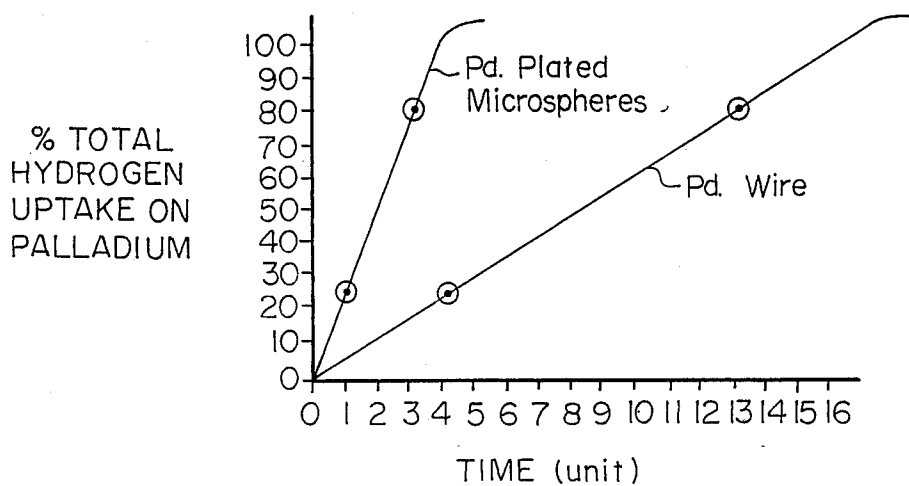
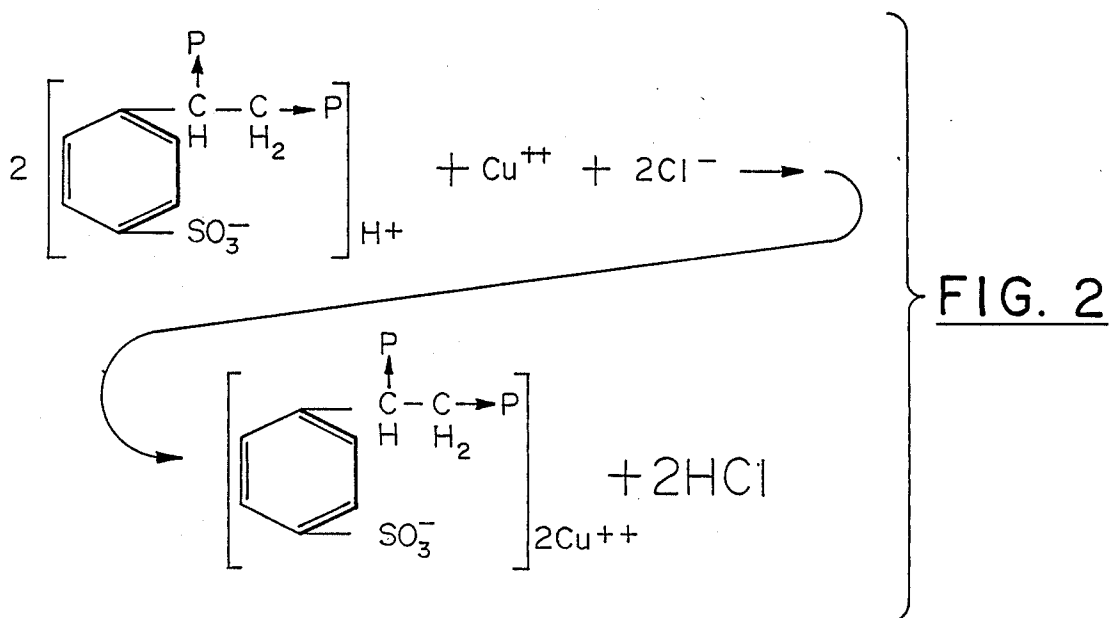


FIG. 3

IMPROVED PROCESS FOR PRODUCING UNIFORMLY PLATED MICROSPHERES

BACKGROUND OF THE INVENTION

1. Field of the Invention

This invention relates generally to metal plating and more particularly to improved an process for the uniform plating of microspheres for use in catalytic processes and electrical applications.

2. Description of Related Art

In U.S. Pat. No. 3,577,324, I described a process and apparatus for plating particles which had as a preferred embodiment the plating of polymeric beads formed from polystyrene cross-linked with divinyl benzene. A solution for bonding copper atoms to such beads was disclosed.

In U.S. Pat. No. 3,787,718, I disclosed the use of plated spherical particles as electronic components. In this patent the forming of additional coatings or platings on the copper layer was also disclosed.

U.S. Pat. No. 2,915,406, Rhoda et al., entitled "Palladium Plating by Chemical Reduction, discloses a number of baths for use in immersion plating of various metals.

The present invention discloses the preparation of resin microspheres having copper salts on the outer portion. These microspheres are separated into batches of substantially uniform sizes and are then plated. By plating microspheres of the same size and density (as determined by Stoke's law) a plating of uniform thickness can be achieved. This uniformly thick plating is essential when the plated microspheres are used in catalytic beds and/or with electric current flowing. Nonuniformly thick platings will result in hot spots which will cause the plating to spall off.

SUMMARY OF THE INVENTION

In a column exchange, a resin in hydrogen form is reacted with chlorosulfonic acid, the resulting microspheres have a sulfonate surface and hydrochloric acid is contained in the solution. The microspheres are washed with deionized water. The sulfonated microspheres are next placed in an aqueous copper chloride solution. The microspheres have copper salts on the surface and hydrochloric acid is contained in the solution. The microspheres are again washed with deionized water. The resulting resin when dried is in the form of microspheres having copper salts on the exterior. These microspheres are separated by passing them through meshes of progressively decreasing size beginning with U.S. sieve cut 16-18 and ending with U.S. sieve cut 25-30. Each such separated group of microspheres is further hydraulically separated to obtain microspheres of sizes identical to ± 0.005 g/cm³. These microspheres are then plated with the electroless copper plating solution described in U.S. Pat. No. 3,577,324 with the required good agitation. After drying and further sorting, these microspheres are given an additional metal plating using the apparatus disclosed in the previously mentioned patent and solutions which will be described herein for various metal platings. Such plated microspheres are useful in electrical applications and in catalytic processes. For example, microspheres having a palladium outer plate have been found to occlude hydrogen in increased quantities and at faster rates than pure palladium wire or palladium plated wire.

It is therefore an object of this invention to provide a process for producing microspheres which have a plating of uniform thickness.

It is also an object of this invention to provide solutions and processes for achieving the metal plating.

In accordance with these and other objects, which will become apparent hereafter, the instant invention will now be described with reference to the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

FIG. 1 depicts the reaction to produce sulfonated cross-linked polymer microspheres.

FIG. 2 depicts the reaction to produce cross-linked polymer microspheres having surface copper salts.

FIG. 3 is a graph showing relative times for total adsorption of hydrogen by palladium coated microspheres and palladium wire.

DETAILED DESCRIPTION OF THE INVENTION

Polystyrene resin is reacted in a column exchange with chlorosulfonic acid yielding sulfonated polystyrene microspheres having hydrogen ions on the outer layer and hydrochloric acid, as shown in FIG. 1. This sulfonation should be limited to a 100 molecular layer depth. If sulfonation is excessive it will be found that the diameter of the microspheres will change when dry microspheres are hydrated. Following this reaction, the sulfonated polystyrene microspheres are washed with deionized water. Next aqueous copper chloride is added to the solution and substitutes for the hydrogen ions in the outer layer, as shown in FIG. 2. The microspheres are again washed with deionized water and dried. The resulting microspheres have copper salts on the exterior. The microspheres are passed through sieves to separate them into batches with each batch containing microspheres of substantially the same size. The largest cut is U.S. Sieve 16-18, followed by 18-20, 20-25 and 25-30 mesh. Each cut is then individually hydraulically separated in a cone having an upwardly laminar water flow. As is well known, in accordance with Stoke's law, microspheres of different densities and size will be found in different layers or zones. The microspheres in each zone are carefully removed separately and are now in fractions which are identical to $+0.005$ grams/cm³. These fractions are then copper coated using the process disclosed in U.S. Pat. No. 3,577,324. The resulting copper coated microspheres perform superiorly as electronic components and in catalytic functions because they do not develop hot spots as occurred with microspheres formed by the previous process. Such hot spots would cause the metal coating to pop off the microspheres.

For many applications a second metal coating is desired. To assure uniformity of coating, the copper coated microspheres are again hydraulically separated to an accuracy of ± 0.0075 grams/cm³.

Second metal platings of various metals have been performed using the apparatus disclosed in U.S. Pat. No. 3,577,324 and the solutions which will now be described.

ELECTROPLATING GOLD PLATING

Solution:	potassium gold cyanide $\text{KAu}(\text{CN})_2$	8-16 g/l
	fluid potassium cyanide KCN	23-39 ml/l

3

-continued

ELECTROPLATING
GOLD PLATING

potassium carbonate K_2CO_3	31-94 ml/l
hydropotassium cyanide $HKCO_3$	23-39 ml/l

This solution is used at a temperature of 130-160 degrees F. with a voltage of 2-5 volts DC and a current density 1-5 amp/ft² with a good upflow and agitation. The resulting plated microspheres have a smooth surface. If a heavy porous surface is desired, the polarity shown in the previously referred to patent is reversed and carbon electrodes in nylon bag covers are used with a current density of 10 amp/ft².

SILVER PLATING

Solution:	silver cyanide $AgCN$	4-5.5 ml/l
	potassium cyanide KCN	78-94 ml/l

This solution is used at a temperature of 70-85 degrees voltage of 4-6 volts DC and a current density of 15-25 amp/ft². The resulting plated microspheres have a smooth surface.

A heavy silver plate requires different parameters and solution.

Solution:	silver cyanide $AgCN$	37.5 ml/l
	potassium cyanide KCN	62.5 ml/l
	potassium carbonate K_2CO_3	15.6 ml/l
	silver metal Ag	27.3 g/l

This solution is used at a temperature of 70-80 degrees with a voltage of 4-6 volts DC and a current density of 5-15 amp/ft².

PLATINUM PLATING

Solution:	chloroplatinic acid H_2PtCl_6	1-2 g/l
	dibasic ammonia phosphate $(NH_4)_2PO_4$	20 g/l
	dibasic sodium phosphate Na_2HPO_4	100 g/l

This solution is used at a temperature of 65-95 degrees F. with a current density of 2-20 amp/ft². A rate of deposition of 4.8 mg/amp/min is achieved or 0.0001 inches/30-60 min/ft². The platinum may be plated over nickel.

PALLADIUM PLATING

Solution:	palladium chloride $PdCl$	50 g/l
	ammonium chloride NH_4Cl	50 g/l

This solution is used at a temperature of 40-50 degrees C. with a current density of up to 10 amps/ft². Note that the voltage should be kept below 1.8 volts DC which is below H_2 production so that the metal surface will not pre-adsorb or occlude hydrogen. A rate of deposition of 33 mg/amp min or 0.000 inches/15 min/ft². The plated surface is a very active polymerization surface so that monomers should be kept away. One volume of palladium will adsorb up to 900 volumes of hydrogen. The palladium can be deposited over nickel.

NICKEL PLATING

Solution:	nickel sulfate $NiSO_4$	156 ml/l
-----------	-------------------------	----------

4

-continued

NICKEL PLATING

	ammonium chloride NH_4Cl	31 ml/l
	boric acid H_3BO_3	31 ml/l

This is used at a temperature of 20-30 degrees C. with a voltage 6-8 volts DC, and a current density of 5-10 amp/ft².

IMMERSION PLATING
PALLADIUM PLATING

Solution:	palladium chloride $PdCl$	4.9 g/l
	hydrochloric acid HCl	250 ml/l

This solution is used at room temperature. This coating is porous and can be sealed by a solution of 1 part ammonia to two parts water.

NICKEL PLATING

Solution:	nickel sulfate $NiSO_4$	62.5 ml/l
	nickel ammonium sulfate $Ni(NH_4)SO_4$	62.5 ml/l
	sodium thiosulfate $Na_2S_2O_3$	62.5 ml/l

This solution was used at room temperature (20-30 degrees C.).

RHODIUM ON COPPER PLATING

Solution:	rhodium chloride $RhCl$	4.9 g/l
	hydrochloric acid HCl	250 ml/l

This solution was used at room temperature in immersion plating.

TIN ON COPPER PLATING

Solution:	tin chloride $SnCl$	19.5 ml/l
	sodium cyanide $NaCN$	195 ml/l
	sodium hydroxide $NaOH$	23.4 ml/l

This solution was used at room temperature in immersion plating.

GOLD ON COPPER PLATING

Solution:	67% potassium gold cyanide $KAuCN$	3.9 ml/l
	sodium cyanide $NaCN$	31 ml/l
	soda ash $NaCO_3$	39 ml/l

This solution was used at 150-180 degrees F. in immersion plating.

SILVER ON COPPER PLATING

Solution:	silver nitrate $AgNO_3$	7.8 ml/l
	ammonia hydroxide NH_4OH	78 ml/l
	sodium thiosulfate $Na_2S_2O_3$	109 ml/l

This solution was used at room temperature in immersion plating.

PLATINUM ON COPPER PLATING

Solution:	platinum chloride $PtCl$	4.9 g/l
	hydrochloric acid HCl	250 ml/l

This solution was used at 150 degrees F. in immersion plating.

ELECTROLESS PLATING

Electroless plating in accordance with the teachings of U.S. Pat. No. 2,874,072 has been performed as will now be described.

COPPER PLATING		
Solution:	copper nitrate $\text{Cu}(\text{NO}_3)_2$	15 g/l
	sodium carbonate Na_2CO_3	10 g/l
	rochelle salts	30 g/l
	sodium hydroxide NaOH	20 g/l
	37% formaldehyde	100 ml/l

PH 11.5, temperature 75 degrees F., 0.1 mil/hr

A high speed, one shot bath coating of copper has been performed.

Solution:	copper sulfate CuSO_4	29 g/l
	sodium carbonate Na_2CO_3	25 g/l
	rochelle salts	140 g/l
	versene "T"	17 g/l
	sodium hydroxide NaOH	40 g/l
	37% formaldehyde	150 g/l

PH 11.5, Temperature 70 degrees C., 0.8 mil/hour

NICKEL PLATING		
Solution:	nickel chloride NiCl	30 g/l
	ammonium chloride NH_4Cl	50 g/l
	sodium citrate Na Cit	100 g/l
	sodium hydrophosphate NaH_2PO_4	10 g/l

PH 10, Temperature 190 degrees F. adjust PH with NH_4OH constantly, 0.3 mil/hr.

PALLADIUM PLATING			
		Still	Moving
Solution:	tetramine palladium chloride	5.4	7.5 g/l
	disodium EDTA	33.6	8.0 g/l
	hydrazine	0.3	
	ammonium hydroxide NH_4OH	350	280 g/l
	temperature	175	95° F.

CATALYTIC SUPPORTED METALS

Only thin metal films are required for catalytic activity. One of the active metal groups for producing surface catalytic reactions is the nickel (58.69), palladium (106.70), white gold (197.20), platinum (195.23) with specific gravities of 8.9, 12.02, 21.45 g/cm^3 , respectively. For example, palladium (Pd) surface will adsorb hydrogen gas. This adsorption will be used as an example to show an improvement in surface activity of metals coated on small stable plastic spheres.

PALLADIUM COATING OF PLASTIC SPHERES

100.000 grams of plastic microspheres were treated as described to produce a flash copper coating. The copper coated microspheres when dry exhibit a static surface charge. Density of microspheres as determined by S.V.S., U.S. Pat. No. 4,196,618 was $1.0550 \pm 0.0005 \text{ gm}/\text{cm}^3$ dry. A 0.1000 gm^3 tube was used in S.V.S. in conjunction with a Metler analytical balance. The microspheres were coated with palladium using three coating techniques, electroplating, immersion plating

and electroless plating. In addition, coils of 100.000 gm, 0.05 mm diameter copper wire were coated using the same technique as the microspheres. All microspheres and wire were coated to give a weight of 20.000 grams of palladium.

TABLE OF RESULTS

PALLADIUM COATING						
			BEADS		WIRE	
WEIGHT	100.00 grams		100.00 grams		100.00 grams	
WEIGHT Pd	20.00 grams		20.00 grams		20.00 grams	
SPECIFIC GRAVITY OF Pd COATING IN GRAMS/ CM^3						
PLATING	E	I	EL	E	I	EL
	11.99	11.40	11.1	12.00	11.95	11.85
	11.85	11.00	10.75			

E = ELECTRODEPOSITION
I = IMMERSION
EL = ELECTROLESS

HYDROGEN LOADING OR Pd SURFACES

As is well known, palladium is noted for its tendency to absorb hydrogen. When finely divided, it takes up about 800 its own volume. See Smith's College Chemistry by James Kendall, The Century Co., 1926, at page 630. Given below are comparative results of adsorption of hydrogen by palladium plated cross-linked polymer microspheres, palladium plated wire and pure palladium wire.

VOLUMES OF HYDROGEN/VOLUME OF Pd								
MICROSPHERES			Pd PLATED WIRE			PURE Pd WIRE		
E	I	EL	E	I	EL	E	I	EL
900	910	950	580	590	610			570
950	975	1050						

1 volume Pd to \times volumes hydrogen

Using specific gravity of Pd at $12.02 \text{ gm}/\text{cm}^3$ and coating weight for Pd volume and standard gas conditions for hydrogen, a volume of metal to volume of hydrogen is given as loading, i.e. where the Pd coating on the beads range from 1.962 to 1.760% of the microsphere volume.

Microspheres range in size from 2 mm to 10 microns.

It is seen that the plated microspheres take up a large volume of hydrogen per unit volume of Pd than either plated wire or pure Pd wire. This shows the improved catalytic nature of metal coated microspheres over plated or pure metal wire. The volume of metal on plated microspheres shows that considerably less metal is required on the microsphere to give improved reactions over the pure metal. Using the Pd - hydrogen uptake as the example.

Extension of the metal coating bead catalytic effects can be extended to cover the isotopes of the reactions shown. See U.S. Pat. No. 3,632,496, where the reactor of FIG. 2 has isolated contact electrodes with an applied electrical potential across the catalyst. Bead bed is Pd/ Hydrogen.

A remarkable result relating to the adsorption of hydrogen by palladium is depicted in FIG. 3. Palladium plated cross-linked polymer microspheres having an outside diameter of essentially 0.8 mm and palladium wire were exposed to hydrogen under standard conditions of temperature and pressure. In unit periods of time as shown in FIG. 3, the microspheres are found to reach maximum uptake in a much shorter period than

the wire. It is believed that the adsorption occurs more rapidly on the surface and the beads present a much higher surface area. In addition, it appears that the thinner the metal plate on the beads, the more rapidly the adsorption occurs, since the hydrogen does not have to penetrate deeply. Moreover, this thin coating does not adversely effect the electrical conduction properties when these microspheres are used as a catalyst in electrochemical or electro induced reactions. Consequently, the shell metal not only produces a greater product yield, but also produces it faster.

Based on the foregoing, the palladium coated microspheres represent an ideal adsorber for hydrogen and its isotopes. Other uses for the plated microspheres of the various metals described above will be apparent to those who typically use such metals as catalysts. The plated microspheres provide enhanced catalytic activity because the surface area is maximized for the weight and volume of the metal.

While the instant invention has been shown and described herein in what is conceived to be the most practical and preferred embodiment, it is recognized that departures may be made therefrom within the scope of the invention, which is therefore not to be limited to the details disclosed herein, but is to be afforded the full scope of the claims so as to embrace any and all equivalent apparatus and articles.

I claim:

1. A process for producing microspheres having uniformly thick metal plating comprising the steps of: forming cross-linked polymer microspheres; separating said microspheres into fractions of uniform size using sieves; further separating each separated fraction into sub-fractions of uniform size and density using hydraulic separation in a cone; removing separately from said cone each subfraction; and plating a selected separated subfraction with metal to a desired thickness.
2. A process in accordance with claim 1 wherein said subfractions are separated to an accuracy of $+0.005 \text{ gm/cm}^3$.
3. A process in accordance with claim 1 wherein: said microspheres are plated with copper.
4. A process in accordance with claim 3 further including: separating said copper coated microspheres into fractions using hydraulic separation in a cone;

- removing separately from said cone each copper coated fraction of microspheres; plating each coated fraction of microspheres separately with a second metal to a desired thickness.
5. A process in accordance with claim 4 wherein: a second metal is taken from the group consisting of gold, silver, platinum, palladium, nickel, rhodium, tin and copper.
 6. A process in accordance with claim 4 wherein: said plating is electroplating.
 7. A process in accordance with claim 4 wherein: said plating is electroless plating.
 8. A process in accordance with claim 4 wherein: said plating is immersion plating.
 9. A process for producing uniformly thick metal plating on crosslinked polymer microspheres comprising the steps of: separating the microspheres into fractions of uniform size using sieves; further separating each separated fraction into sub-fractions of uniform size and density using hydraulic separation in a cone; removing separately from said cone each subfraction; and plating a selected separated subfraction with metal to a desired thickness.
 10. A process in accordance with claim 9 wherein said subfractions are separated to an accuracy of $+0.005 \text{ gm/cm}^3$.
 11. A process in accordance with claim 9 wherein: said microspheres are plated with copper.
 12. A process in accordance with claim 11 further including: separating said copper coated microspheres into fractions using hydraulic separation in a cone; removing separately from said cone each copper coated fraction of microspheres; plating each coated fraction of microspheres separately with a second metal to a desired thickness.
 13. A process in accordance with claim 12 wherein: said second metal is taken from the group consisting of gold, silver, platinum, palladium, nickel, rhodium, tin and copper.
 14. A process in accordance with claim 12 wherein: said plating is electroplating.
 15. A process in accordance with claim 12 wherein: said plating is electroless plating.
 16. A process in accordance with claim 12 wherein: said plating is immersion plating.
- * * * * *

55

60

65